



| The European Synchrotron

MEDSI 2016

MECHANICAL ENGINEERING DESIGN OF SYNCHROTRON
RADIATION EQUIPMENT AND INSTRUMENTATION



THERMAL STABILITY OF THE NEW ESRF EXTREMELY BRILLIANT SOURCE

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Instabilities

Instabilities

1. Permanent static errors from the origin
2. Permanent variable errors (quick effects)
3. Errors triggered by beam operation
4. Long period errors

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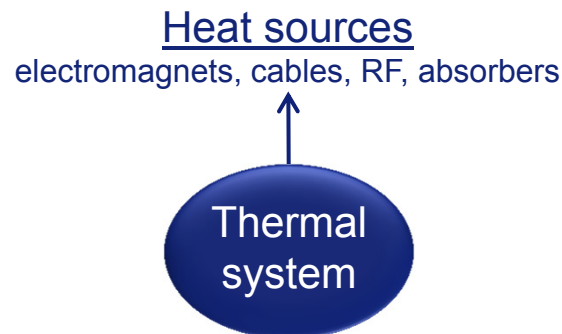
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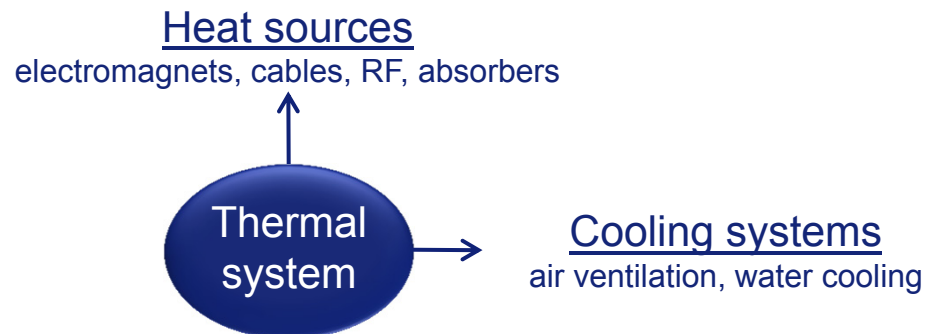
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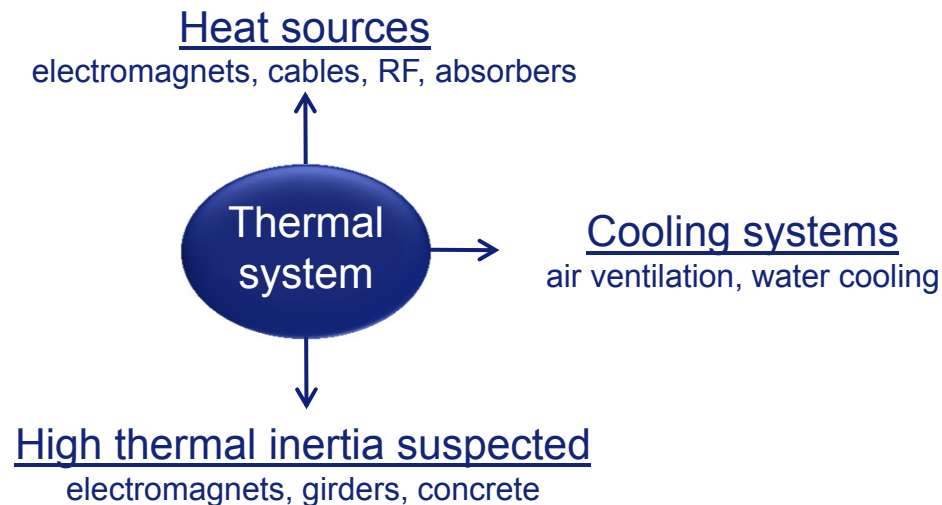
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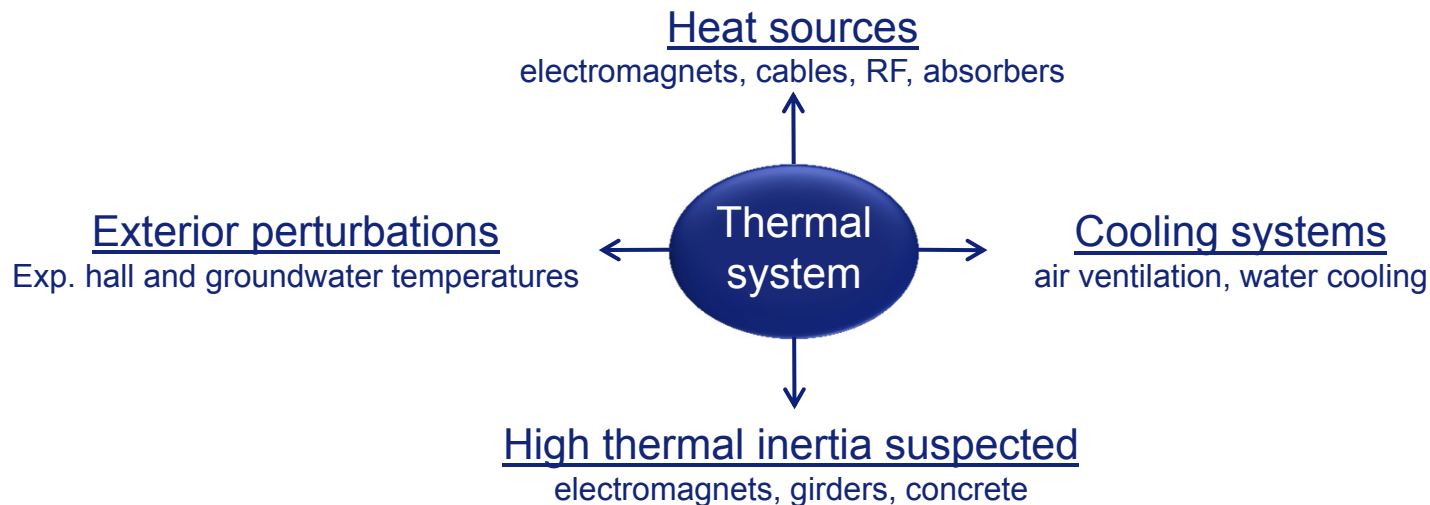
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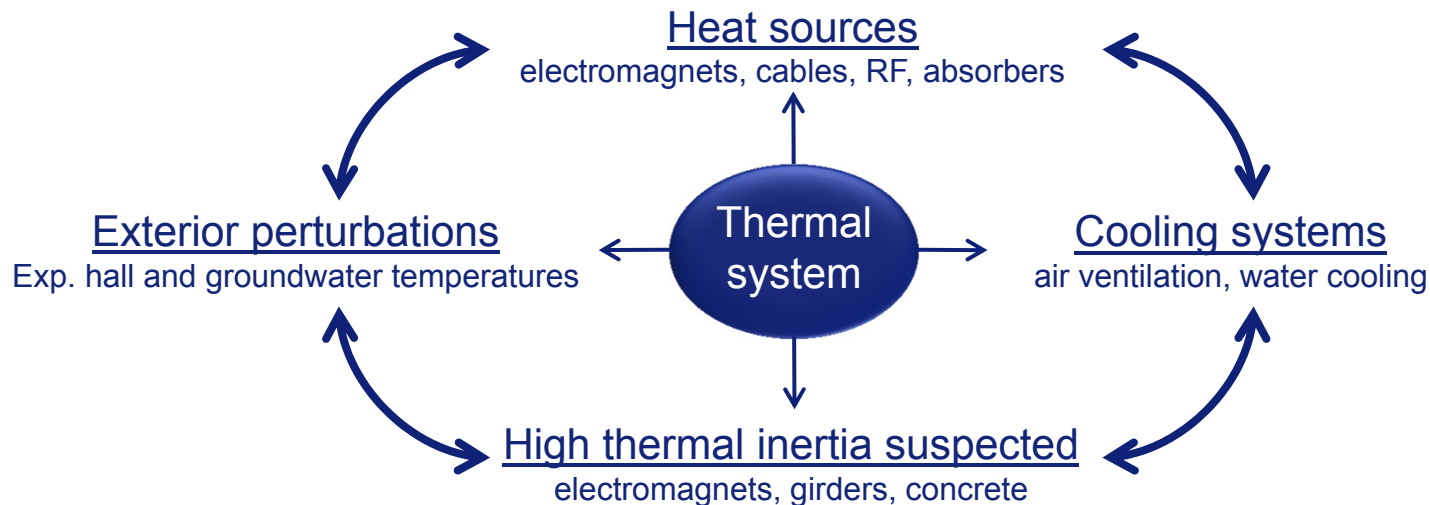
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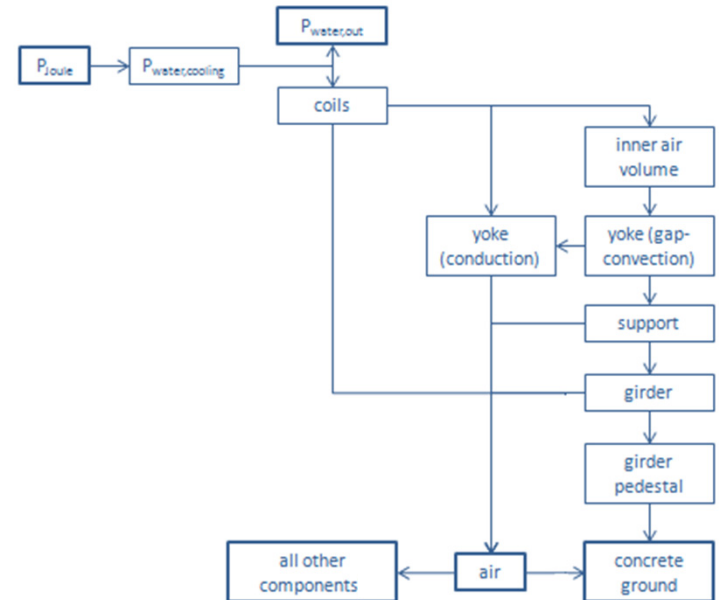


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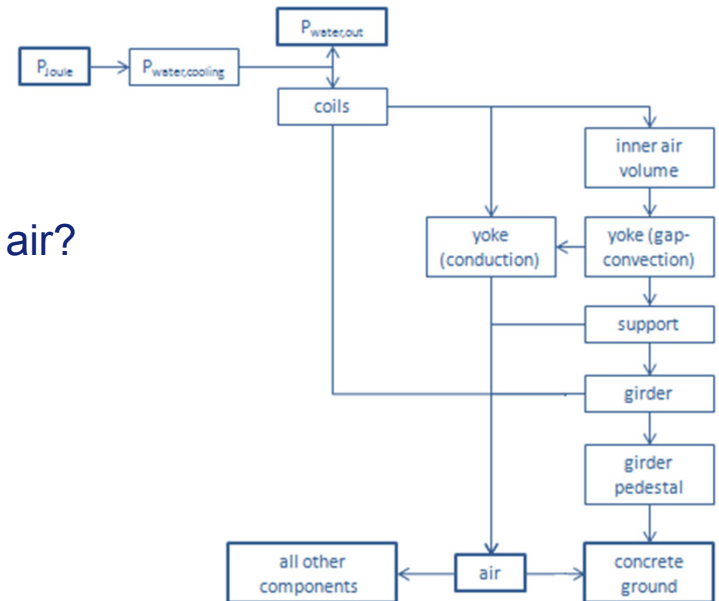
EBS ELECTROMAGNETS

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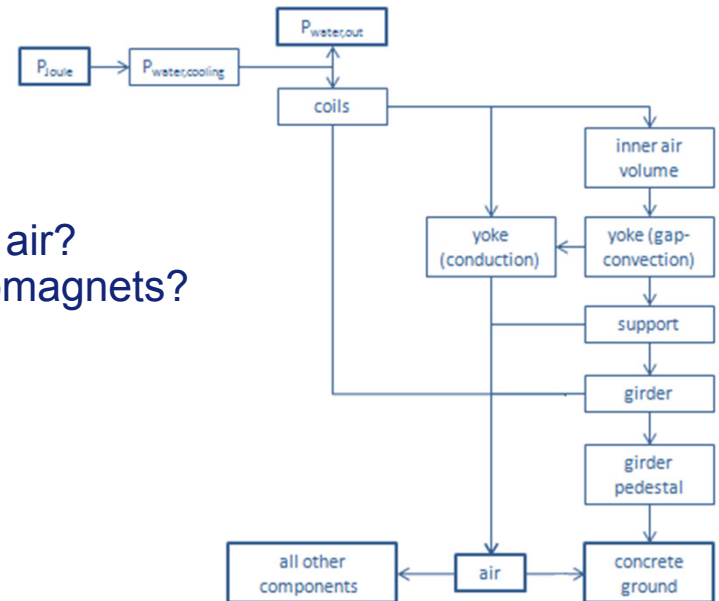
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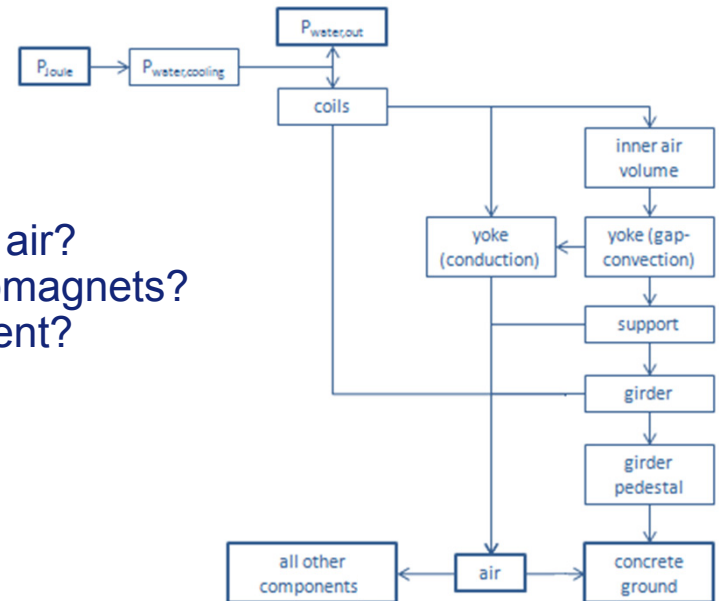
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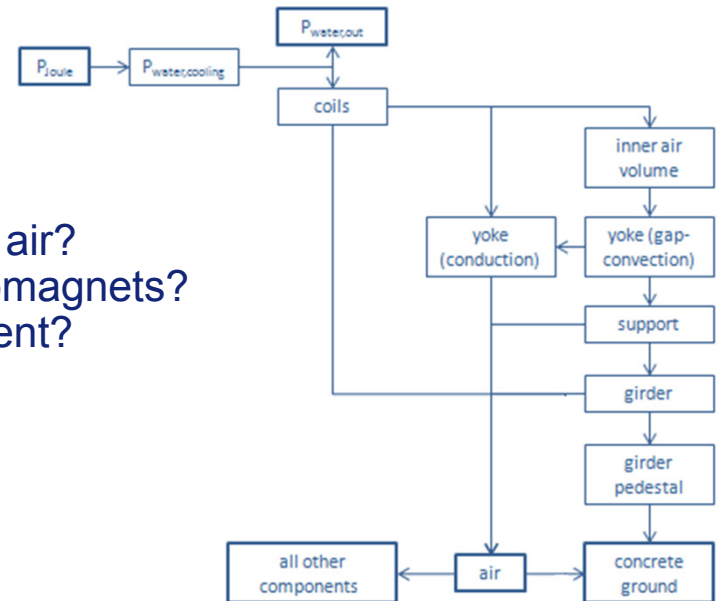
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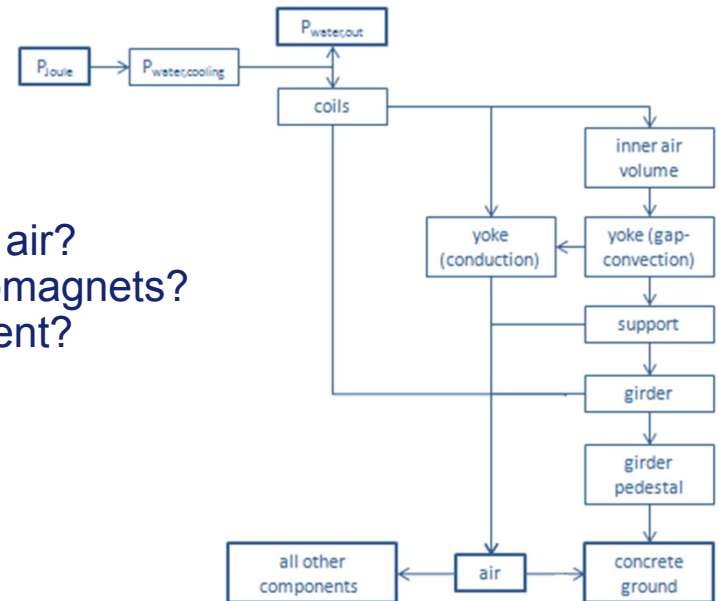
➡ FEA exploring work



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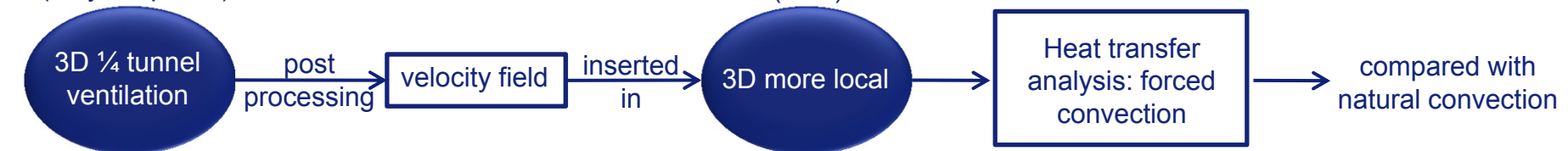
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very first CFD model
(very simplified)

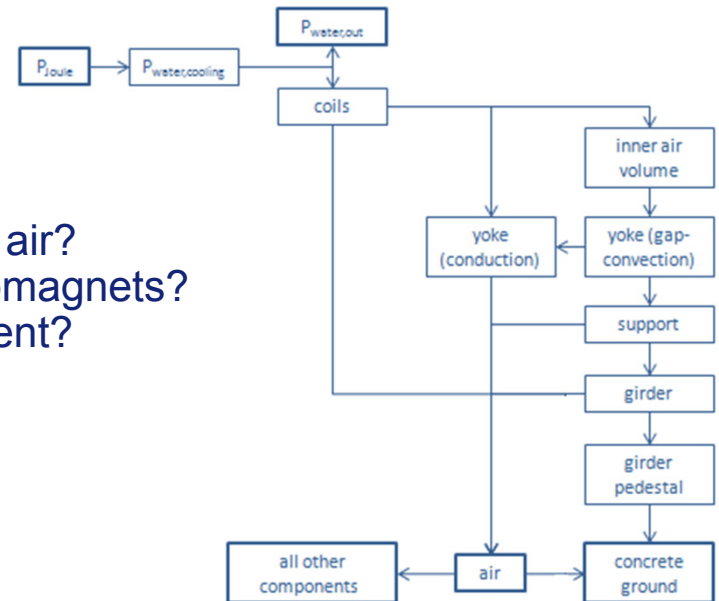
second CFD and thermal model
(finer)



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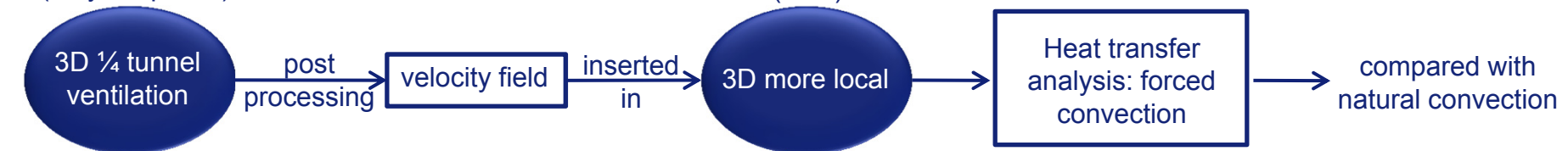
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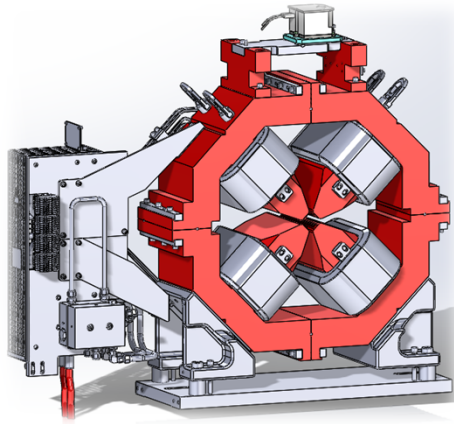
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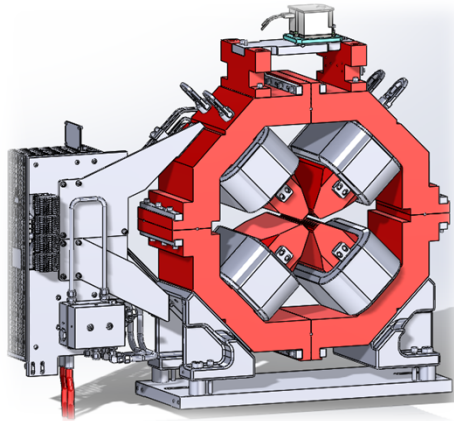
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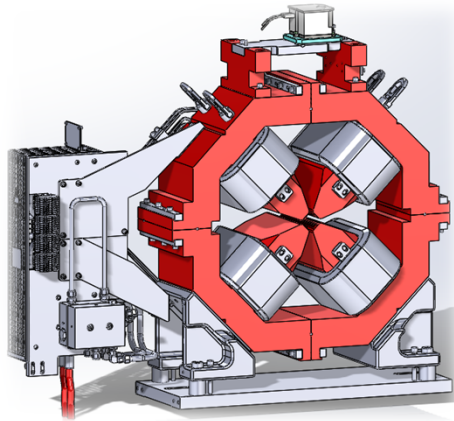
Inner volume of electromagnets: natural convection is predominant

EBS QUADRUPOLE





- Each coil dissipates 500W of heat (2000W total)
- Coils are water cooled in parallel
 - 0.45L/min
 - T_{inlet} = 24°C
 - T_{outlet} = 40°C
- Air: only natural convection is considered
 - T_{ambient} considered constant at 24°C



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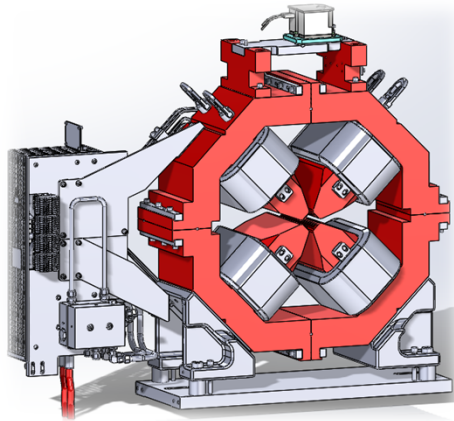
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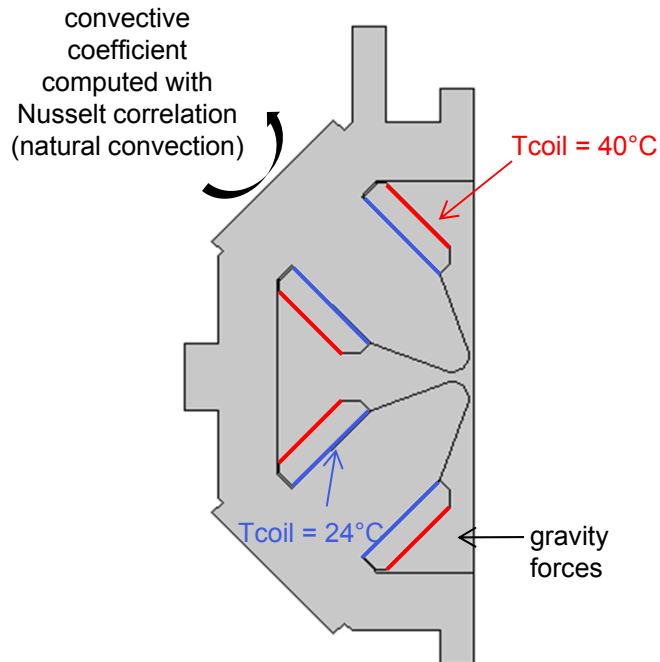
➡ Even simplified, a full 3D model remains too heavy for CFD

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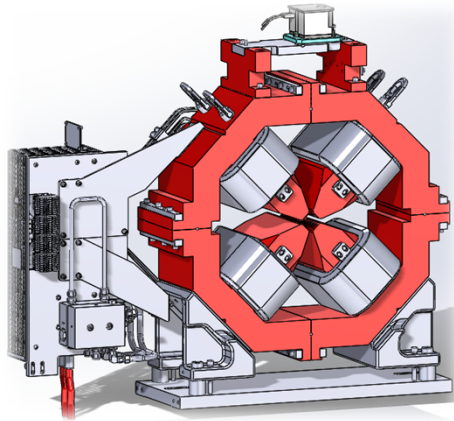


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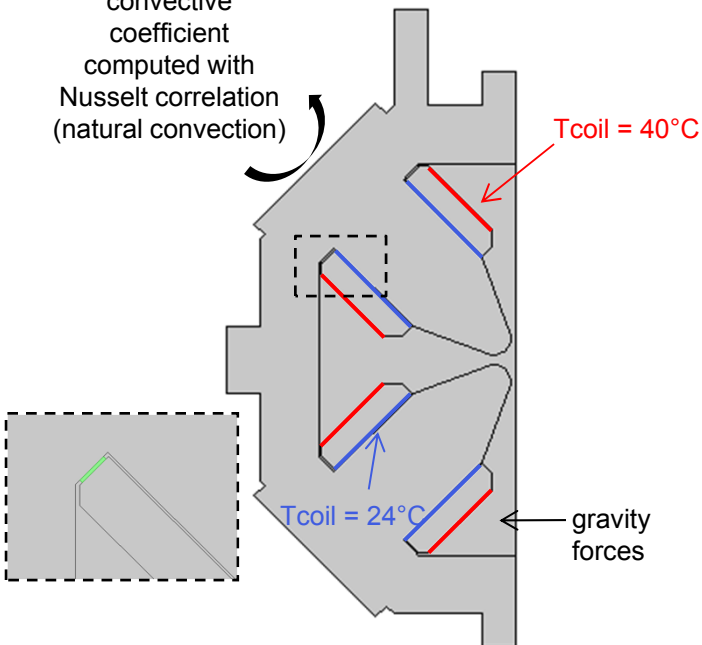
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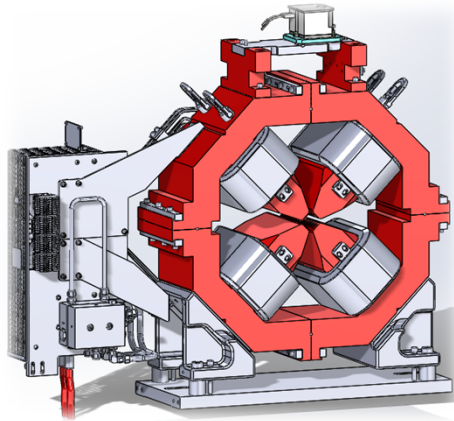
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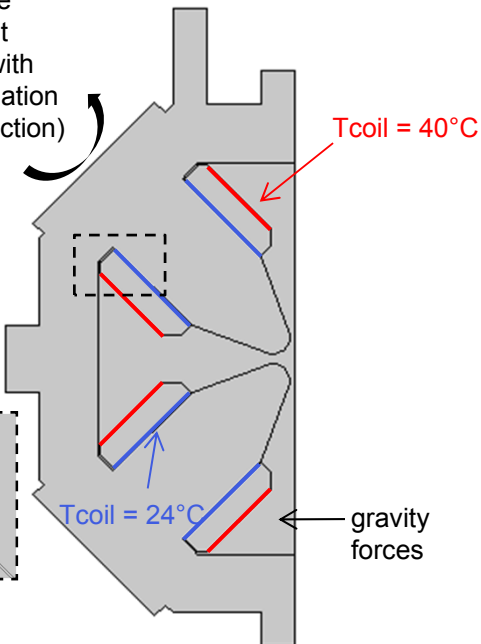
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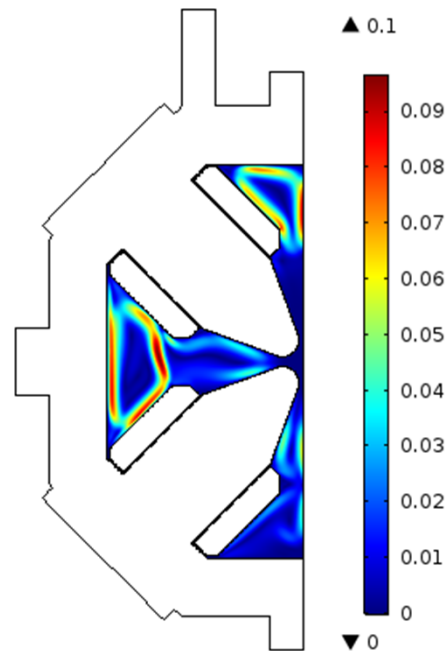
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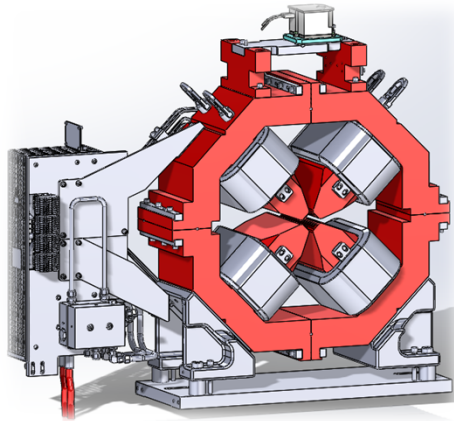
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velocity field (m/s) - steady state



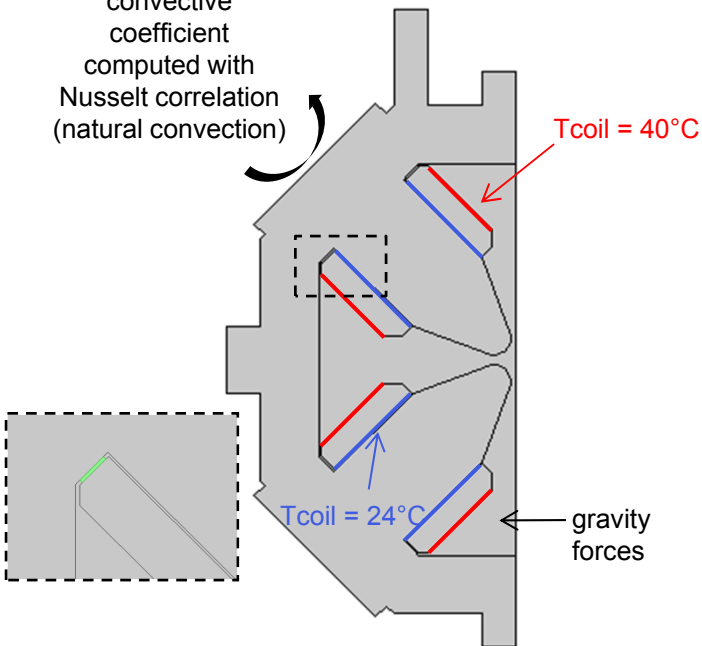
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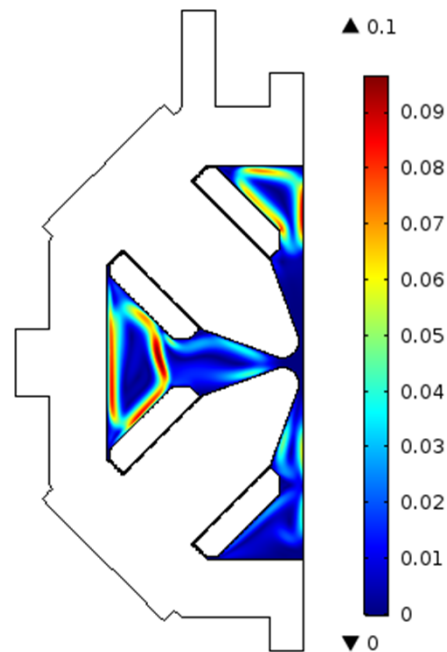
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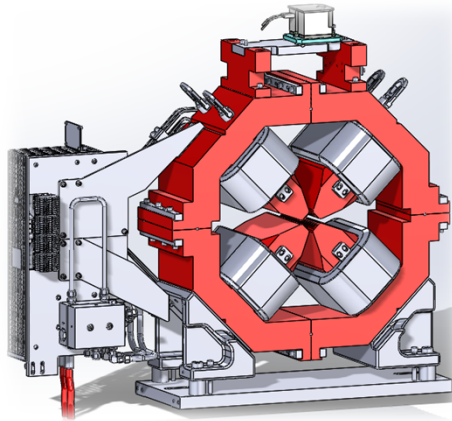


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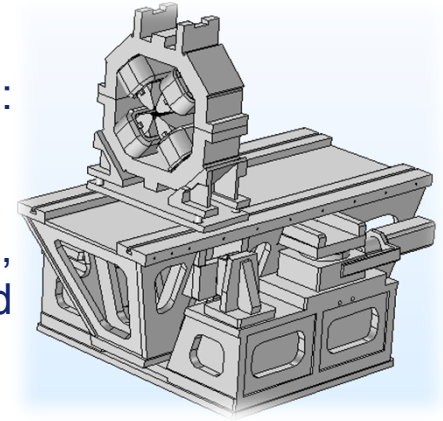


local convective coefficients
computed all along inside
surfaces of the quadrupole

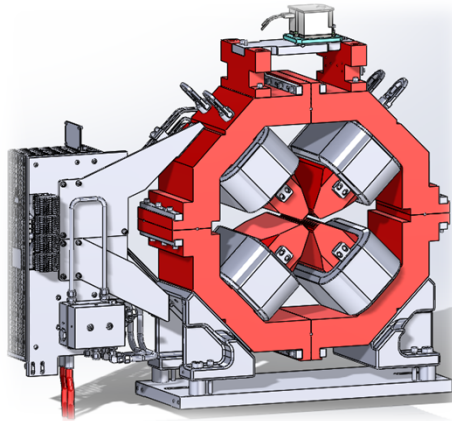
EBS QUADRUPOLE – TEMPERATURE



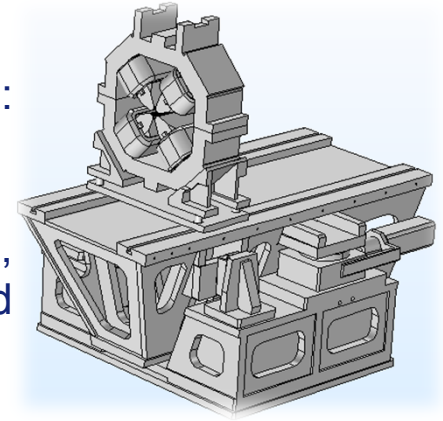
- Local convective coefficients from 2D model: into a 3D model
- A part of the girder is modeled
- Same boundary conditions than 2D model, but without CFD and assuming ground temperature at 24°C
- Initially, quadrupole at 24°C



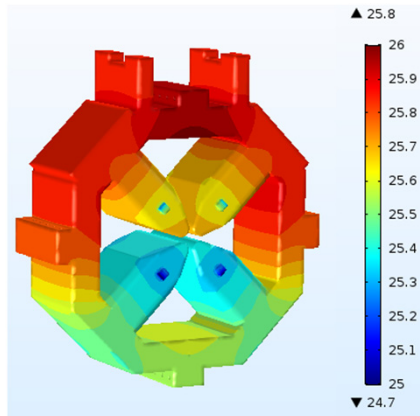
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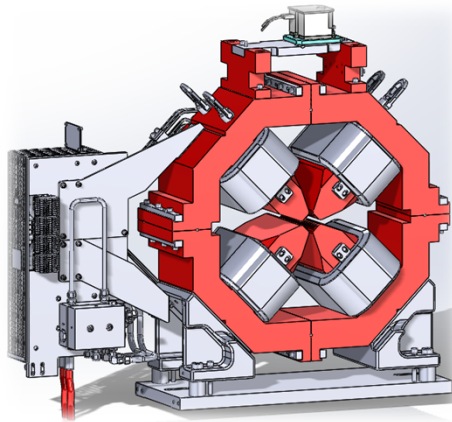


Temperature field [°C]

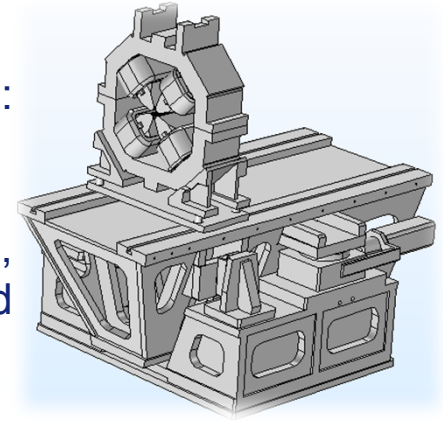


Average temperature: 25.4°C (+1.4°C from initial value)

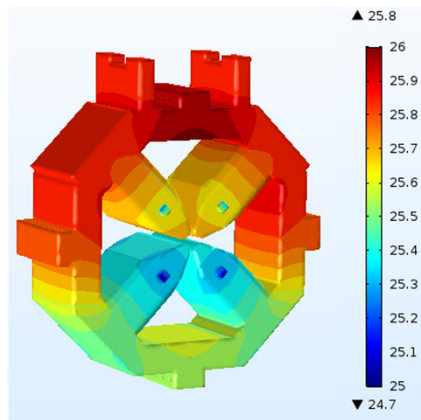
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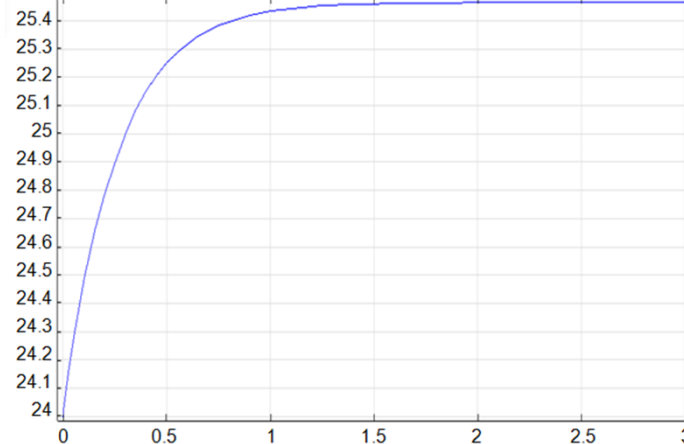


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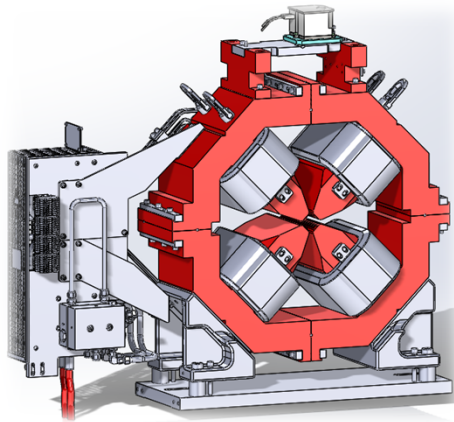
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Average temperature (yoke & poles) [°C] against time [d]

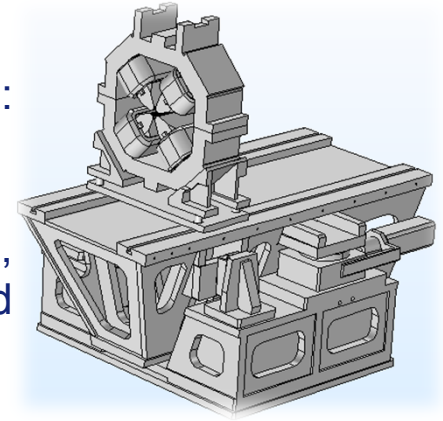


Steady state reached after: $5\tau \sim 1.5$ days
Time constant $\tau \sim 0.3$ day

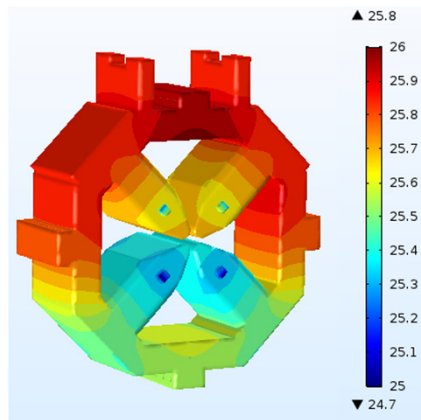
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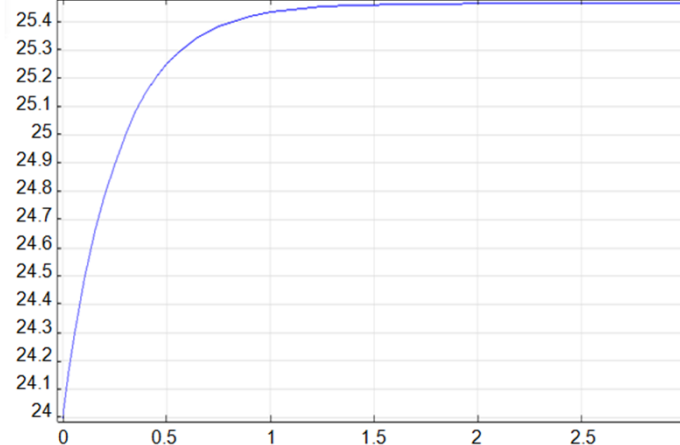


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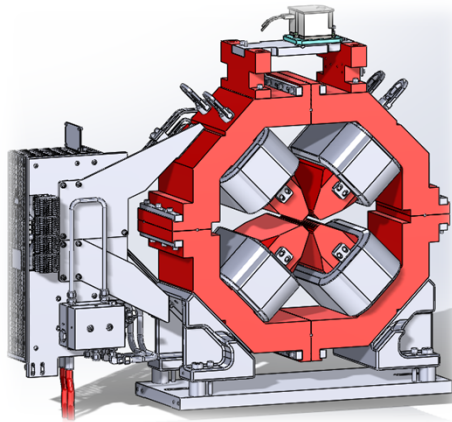


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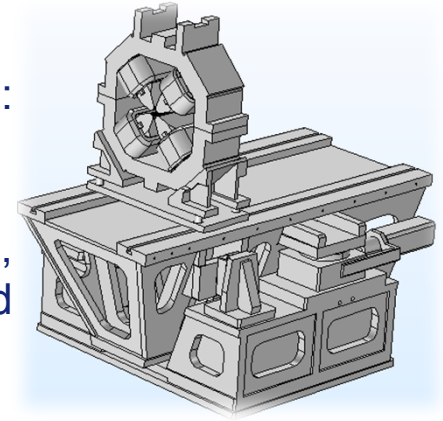
➡ time constant of ~ 0.3 day

➡ temperature increase by $\sim 1^\circ\text{C}$

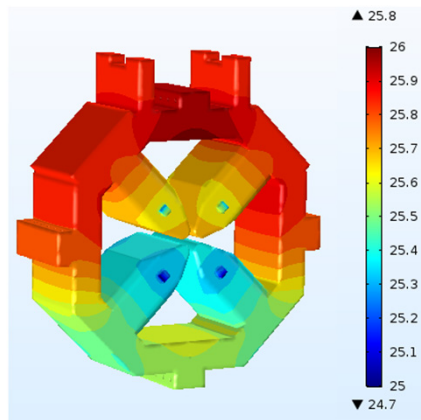
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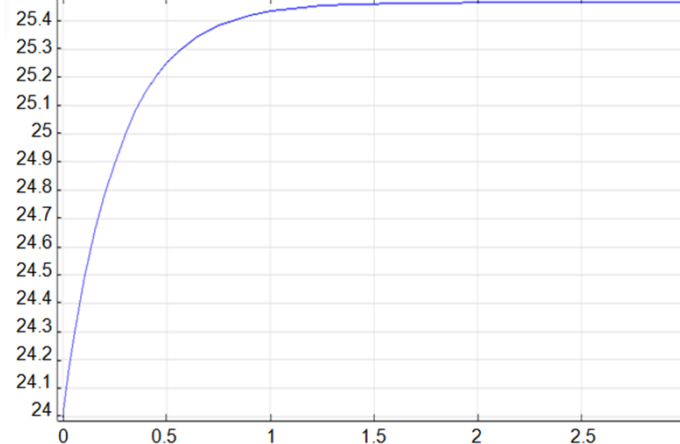


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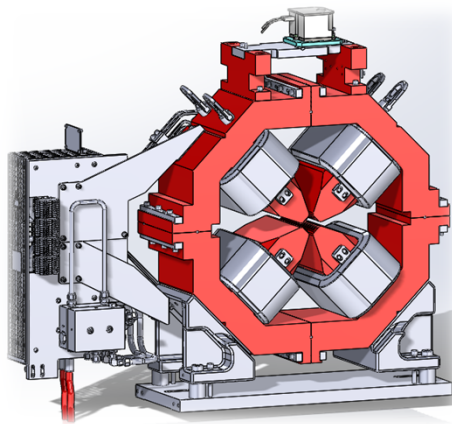


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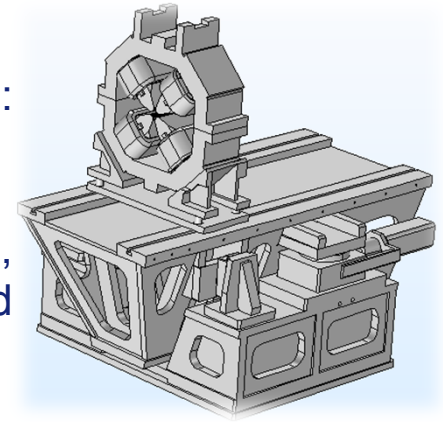
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observed experimentally ☺

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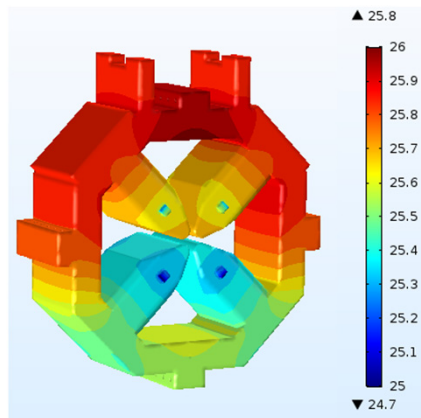
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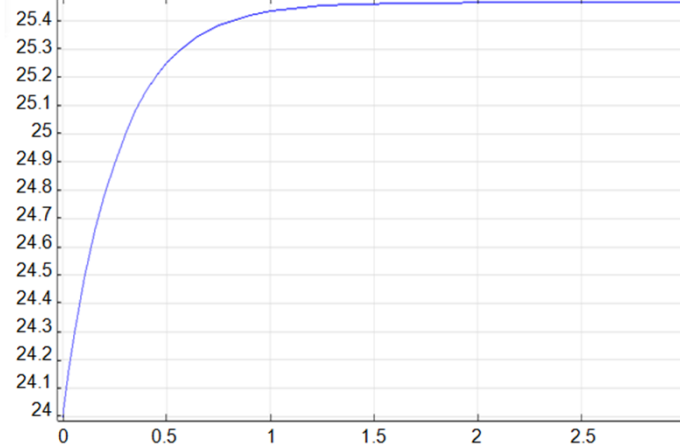


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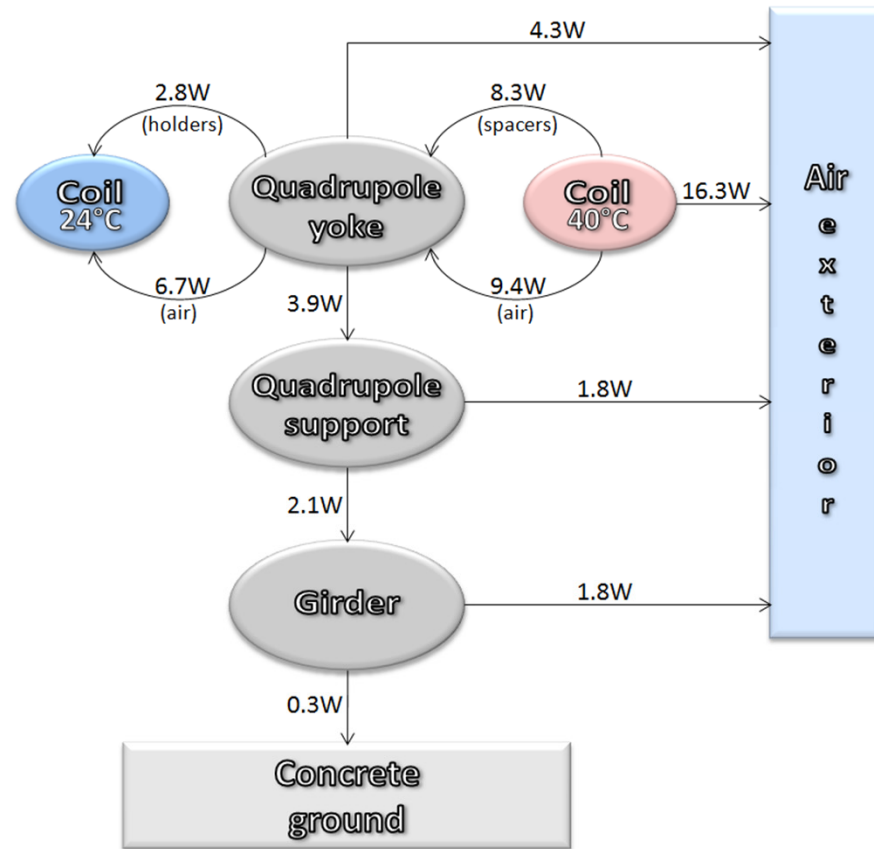
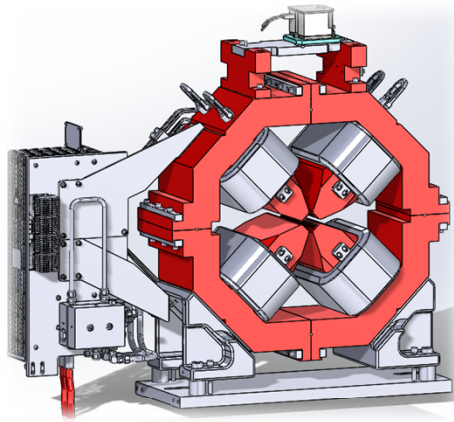


Steady state reached after: $5\tau \sim 1.5$ days
Time constant $\tau \sim 0.3$ day

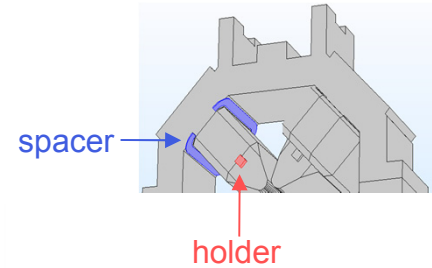
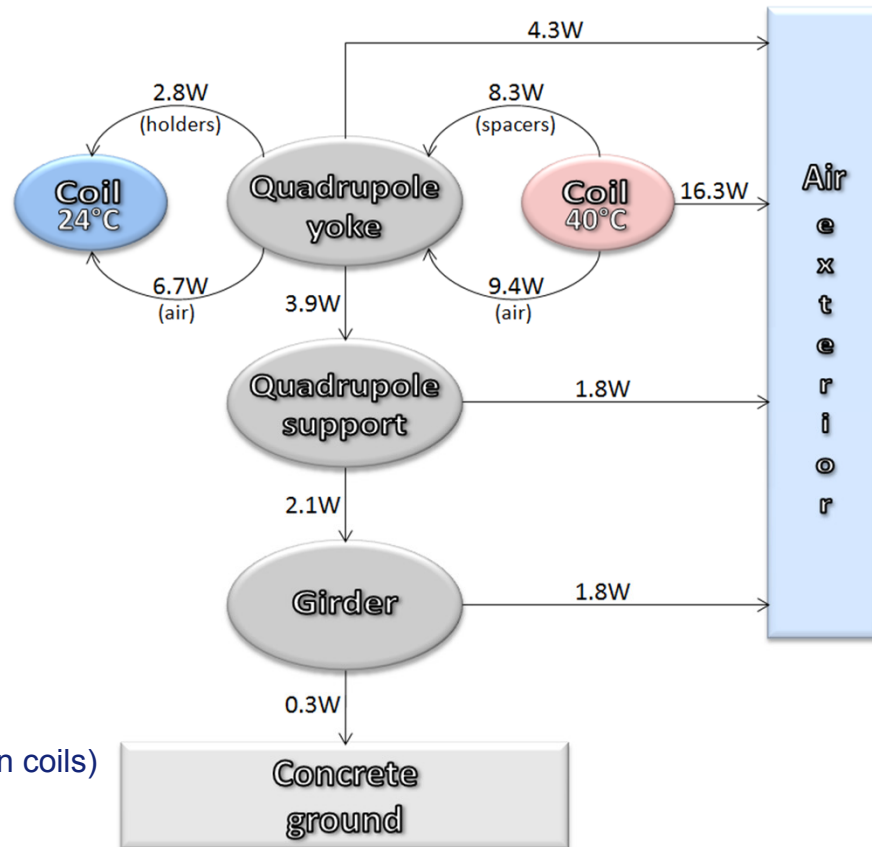
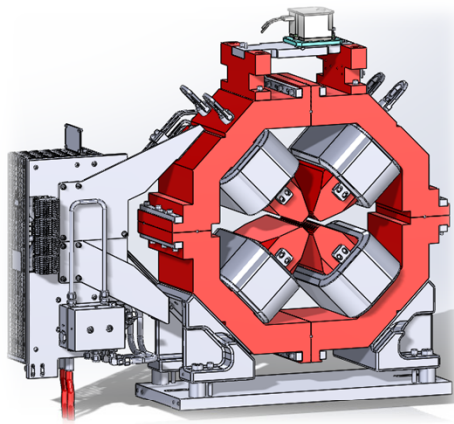
➡ time constant of ~ 0.3 day
observed experimentally ☺

➡ temperature increase by $\sim 1^\circ\text{C}$
not observed experimentally ☹
(actually it is $+3^\circ\text{C}$)

EBS QUADRUPOLE – HEAT BALANCE

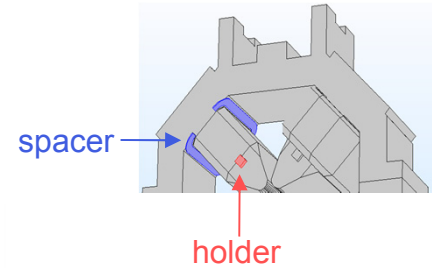
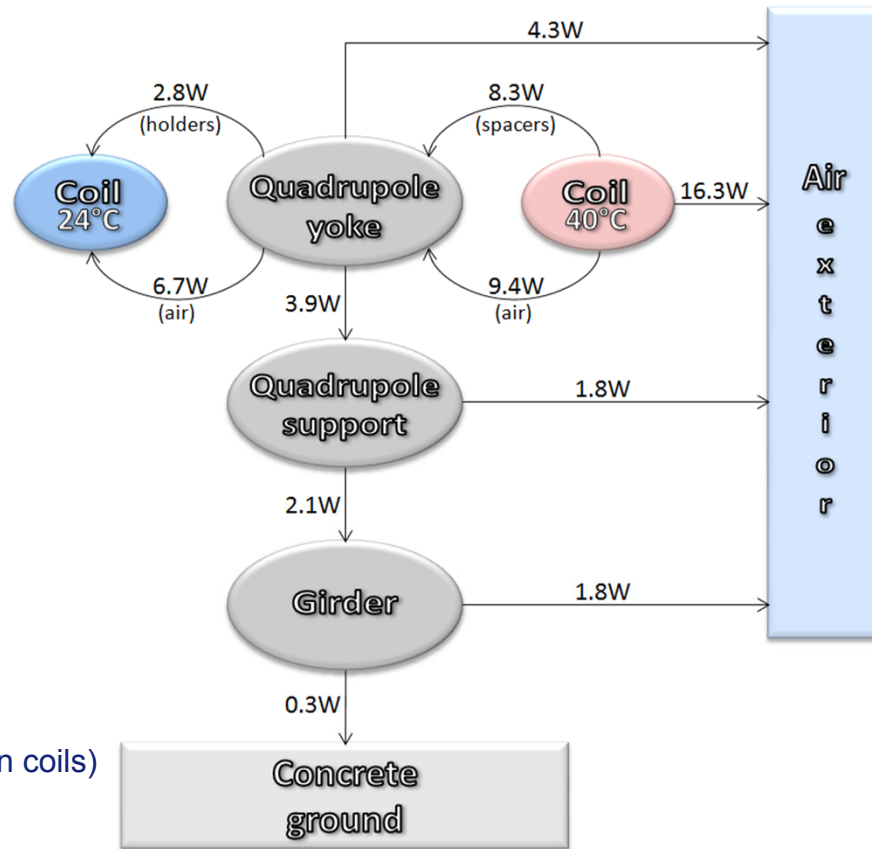
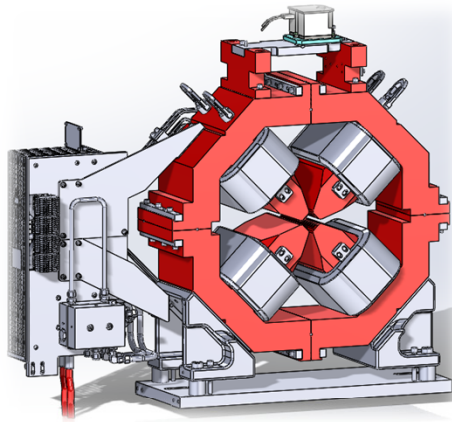


EBS QUADRUPOLE – HEAT BALANCE



- Coils ↔ Quadrupole:
17.7W in
 - 46.9% from spacers
 - 53.1% from air
- 9.5W out
 - 29.5% from holders
 - 70.5% from air
- 24.2W in air (1.2% of the total heat in coils)
- 0.3W in ground

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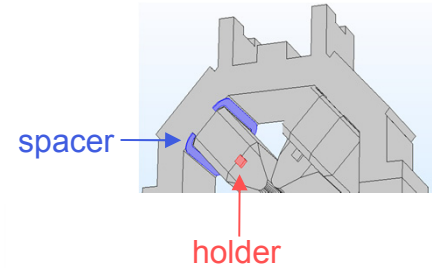
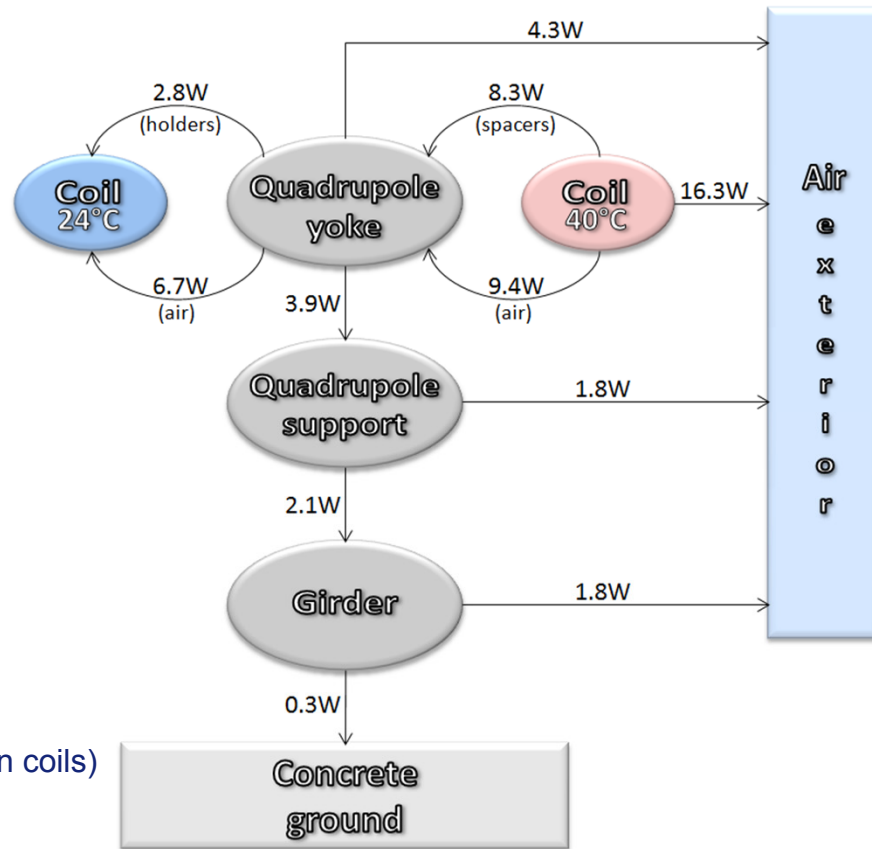
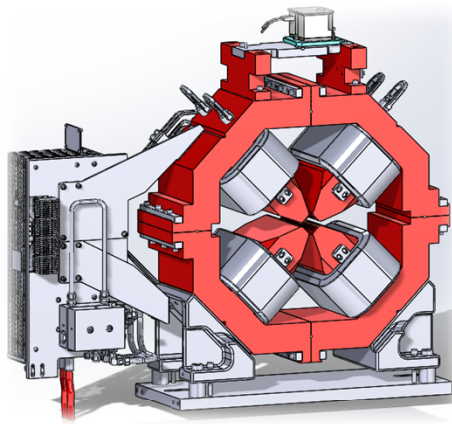
FEA

EXP.

Tav. +1°C

Tav. +3°C

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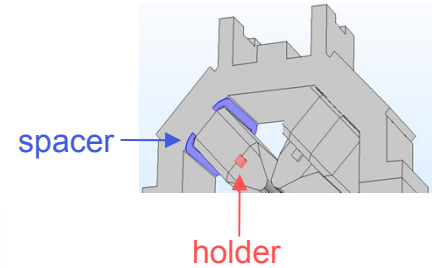
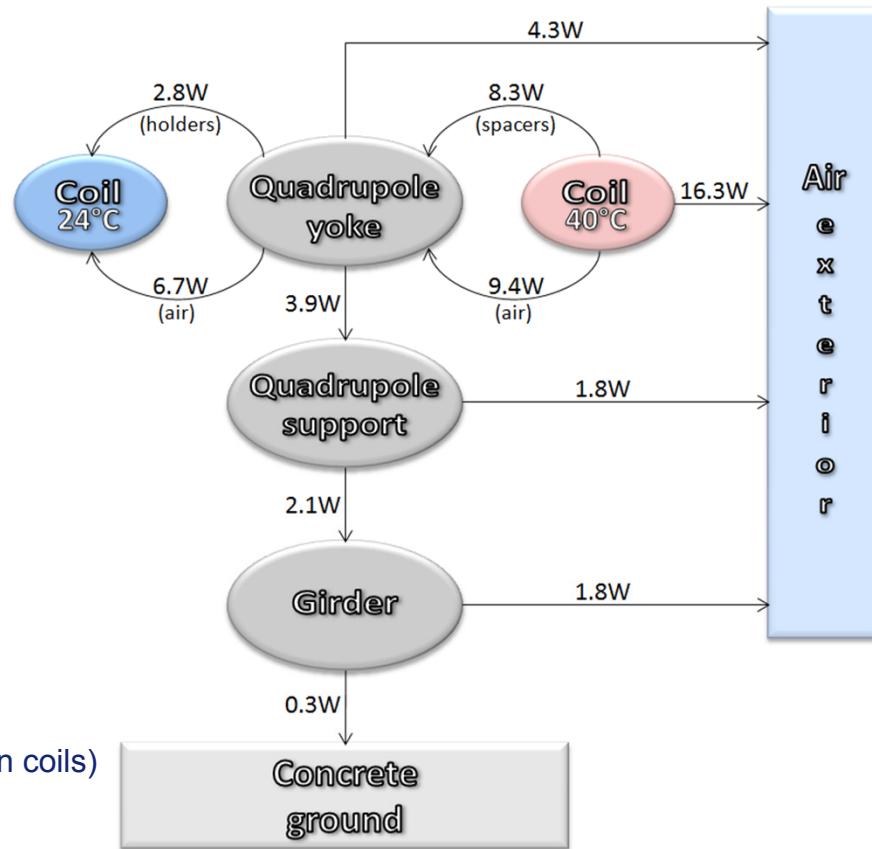
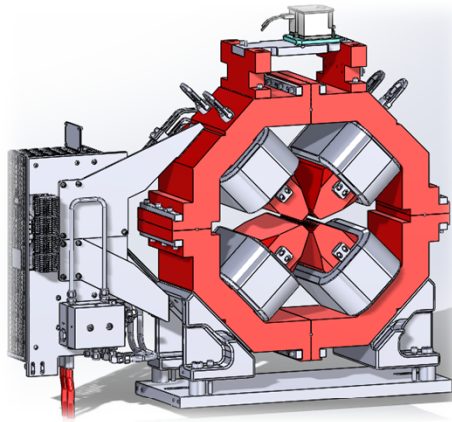
Tav. +1°C

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1% of heat in air

4% of heat in air

EBS QUADRUPOLE – HEAT BALANCE



spacer

holder

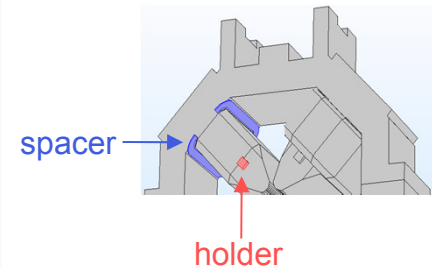
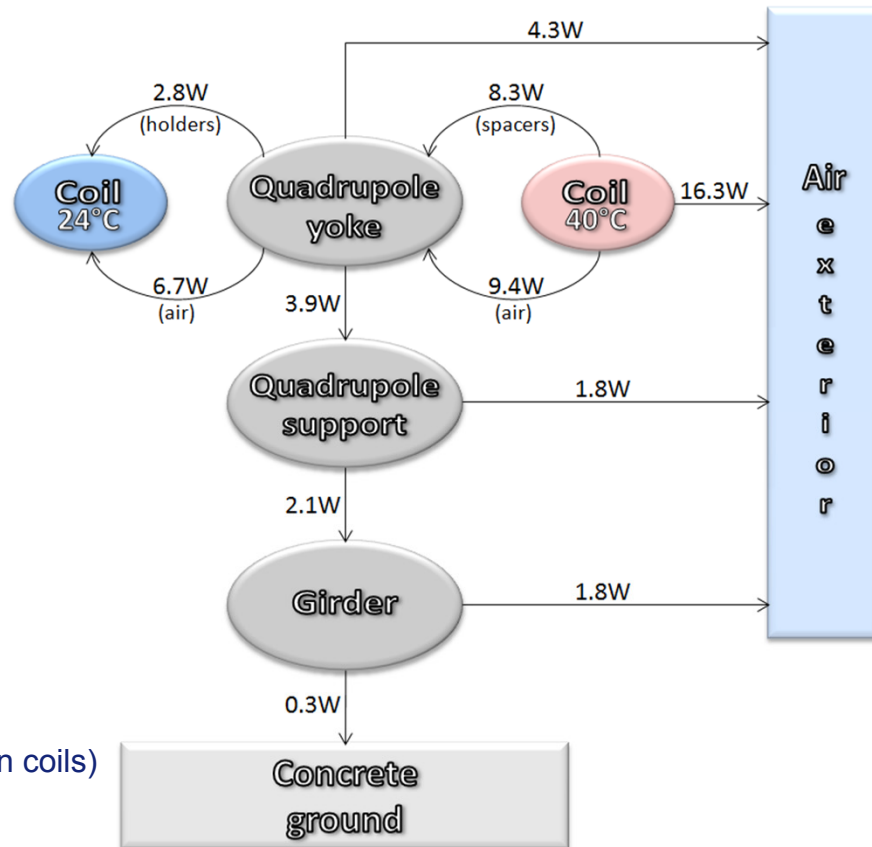
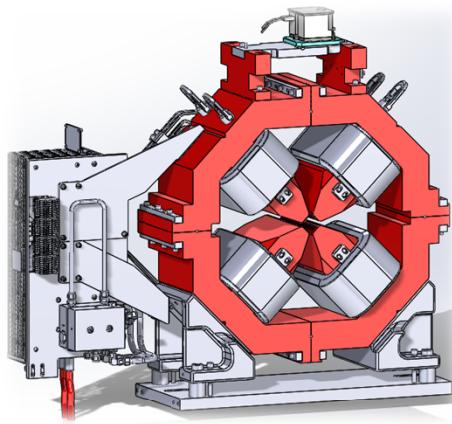
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FEA	EXP.
Tav. +1°C	Tav. +3°C
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EXP. magnet more than twice as deep as the FEA one

EBS QUADRUPOLE – HEAT BALANCE



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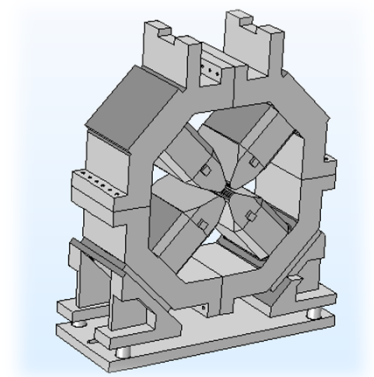
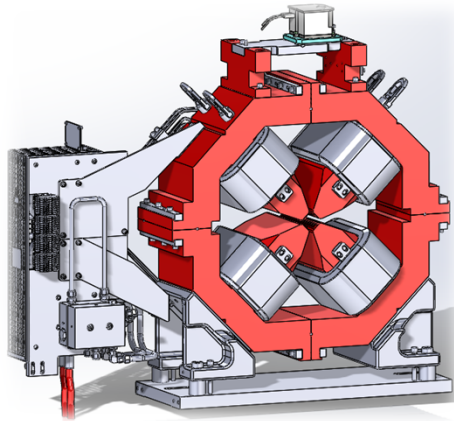
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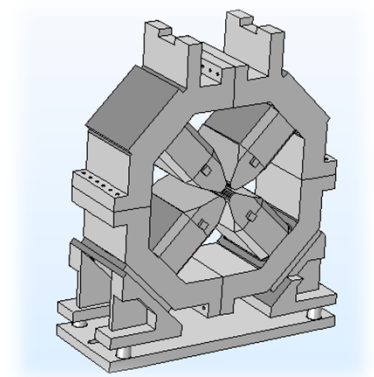
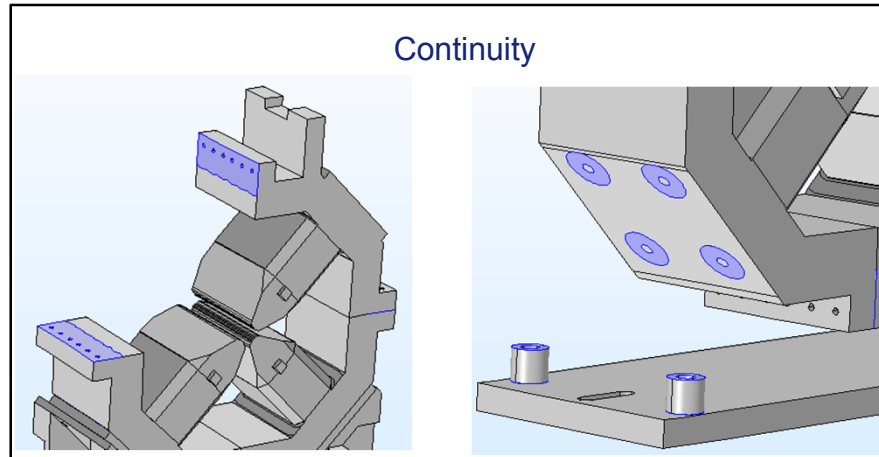
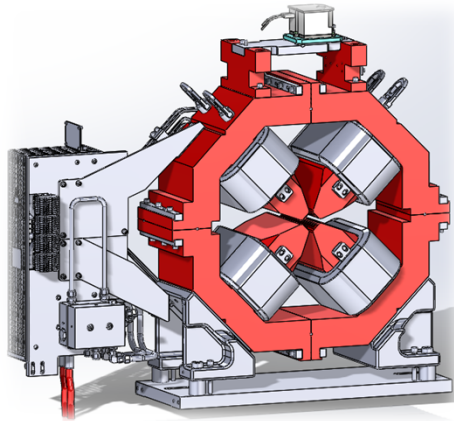
EXP. magnet more than twice as deep as the FEA one

more heat added to quadrupole
more investigations to do

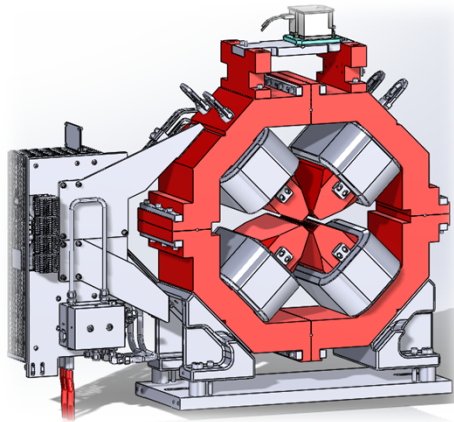
EBS QUADRUPOLE – THERMOMECHANICAL DISPLACEMENTS



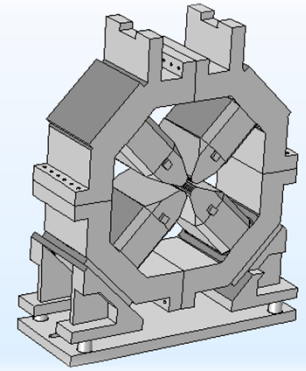
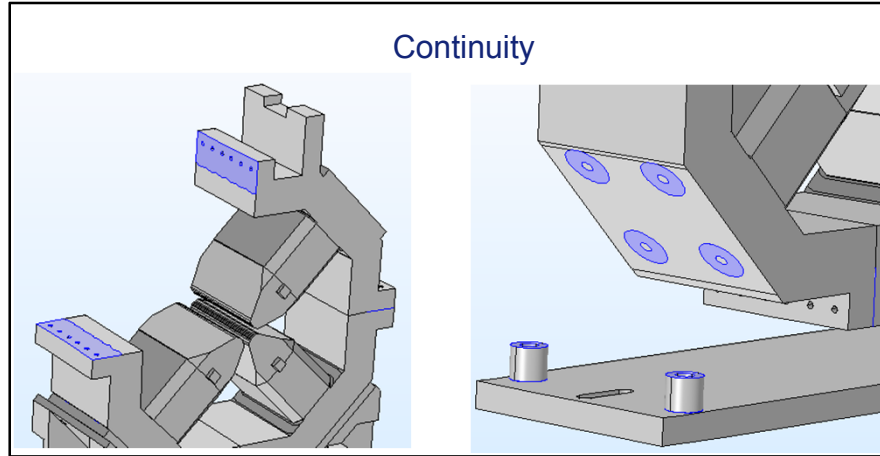
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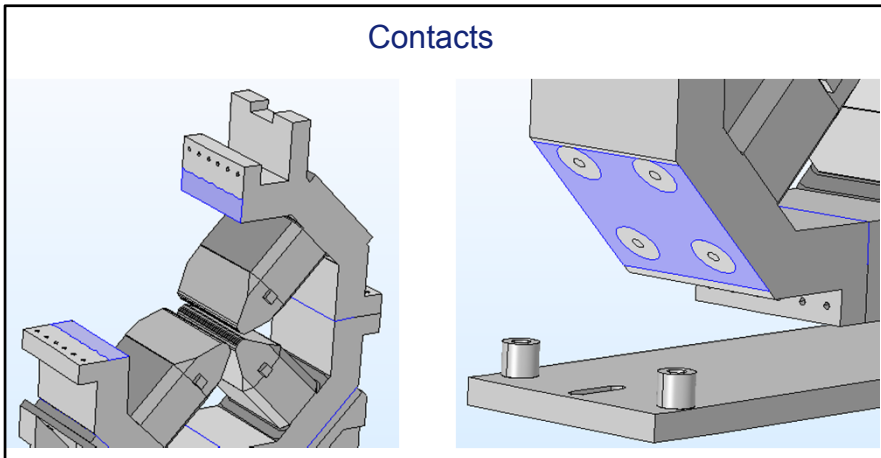
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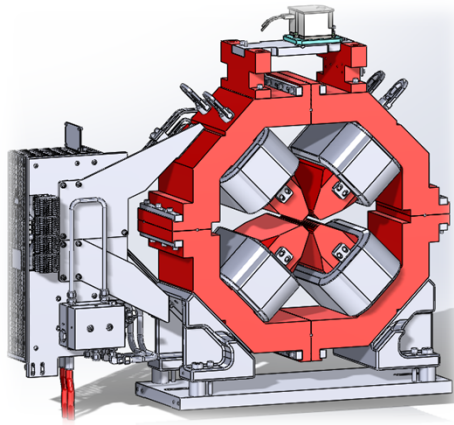
Continuity



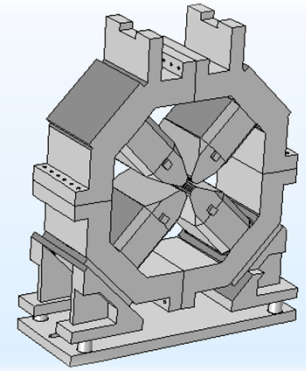
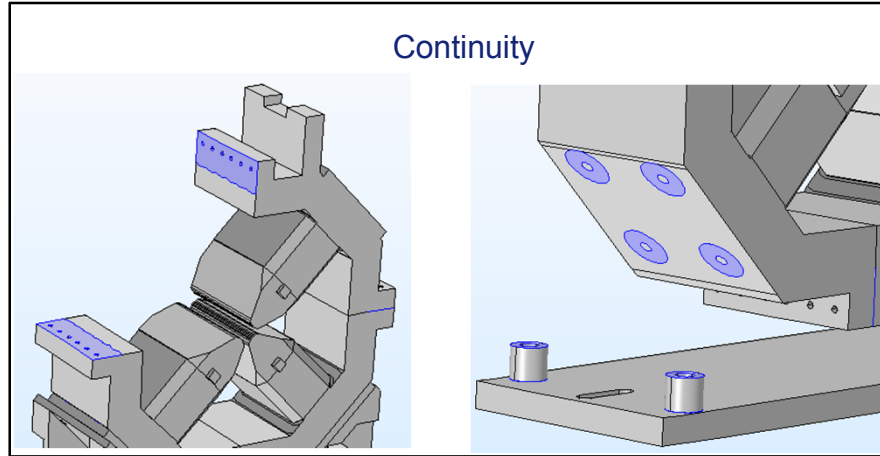
Contacts



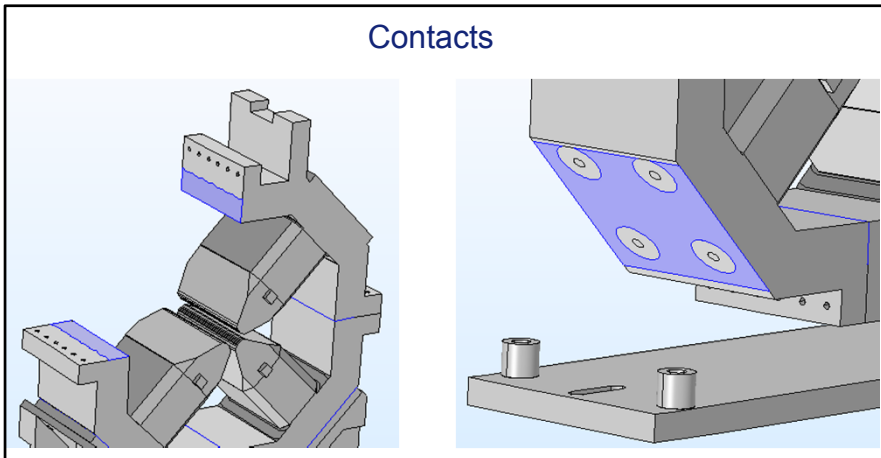
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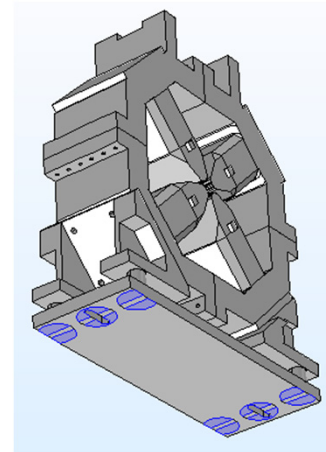
Continuity



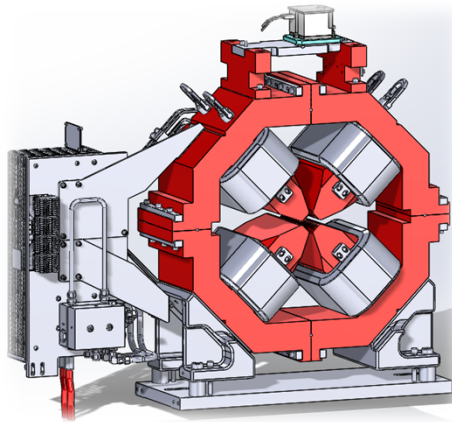
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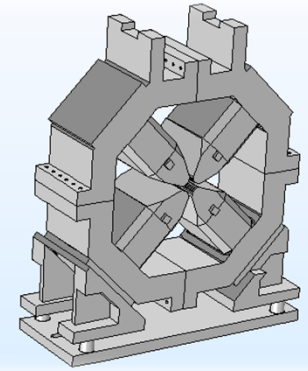
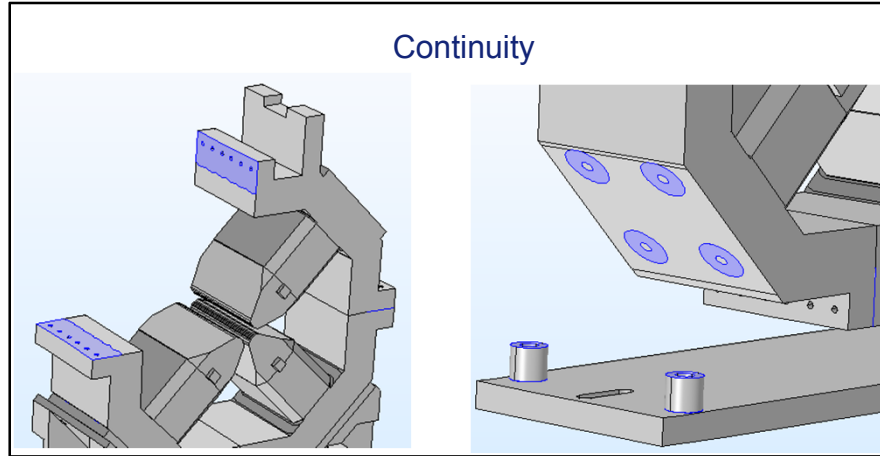
Displacement = 0



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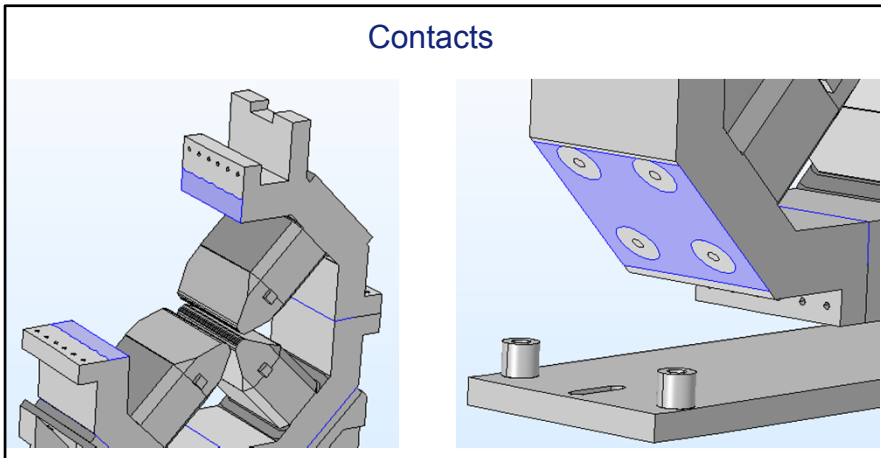


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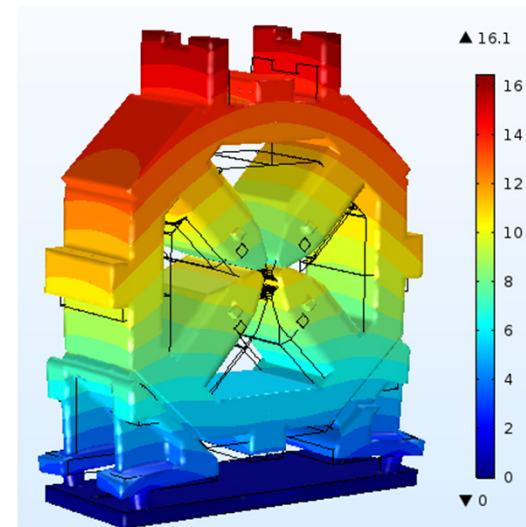
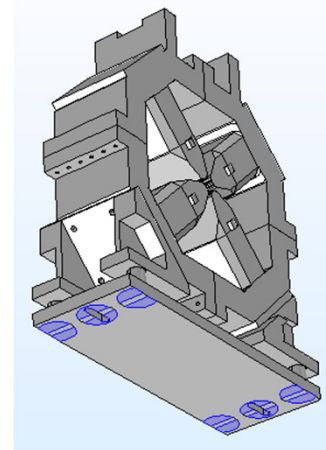


Total displacements [μm]

Contacts



Displacement = 0



GIRDER MOCK-UP



Full scale mock-up girder prototype with power cables inside



GIRDER MOCK-UP



Full scale mock-up girder prototype with power cables inside
Why cables inside the girder?



GIRDER MOCK-UP



Full scale mock-up girder prototype with power cables inside
Why cables inside the girder?

└→ mainly for space savings reasons



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But:

- might be dangerous (girder deformation due to the heat)
- difficult to implement



GIRDER MOCK-UP



Full scale mock-up girder prototype with power cables inside

Why cables inside the girder?

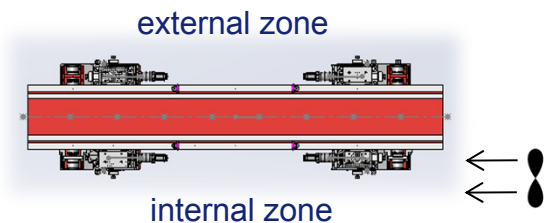
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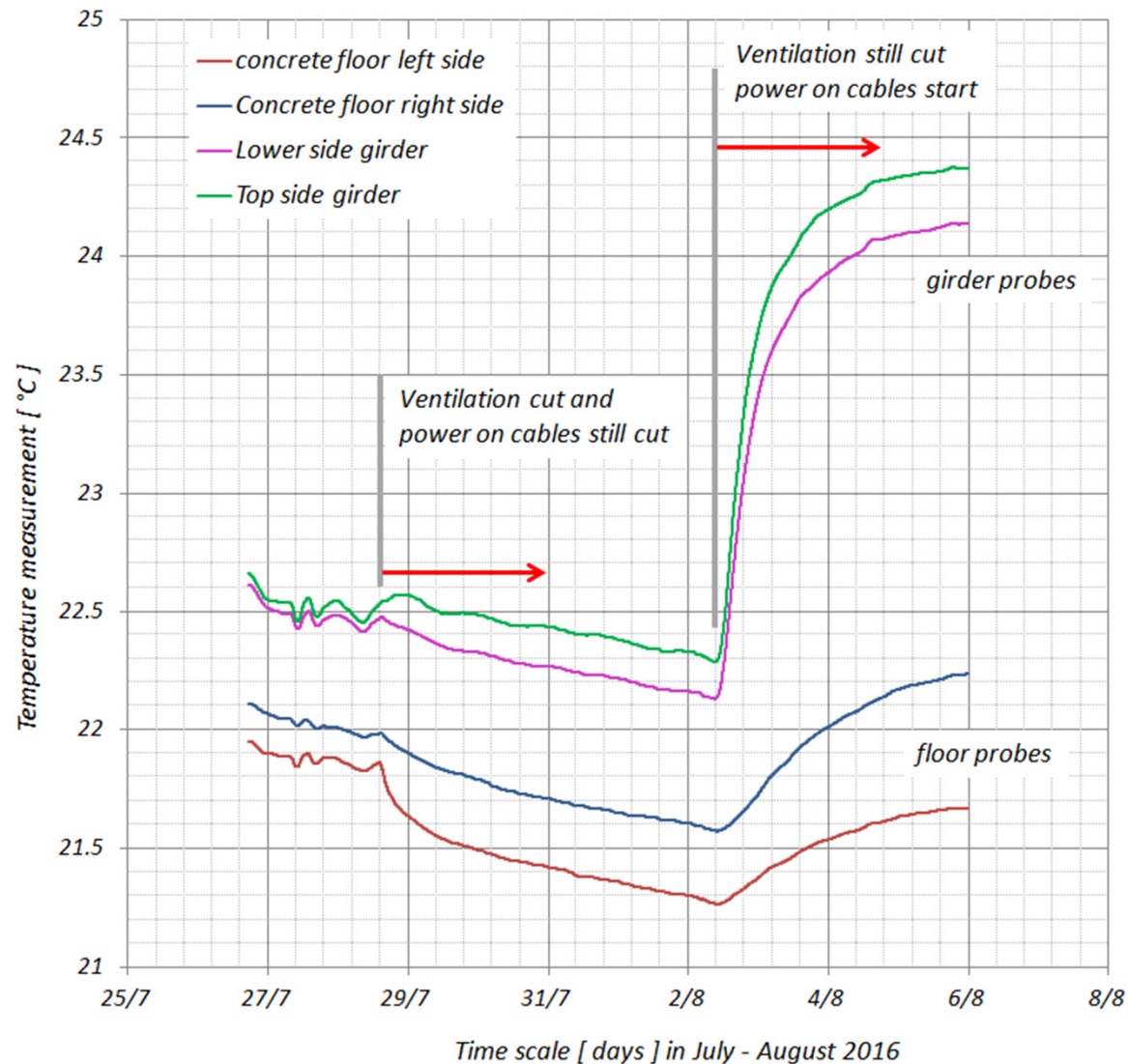
Mock-up:

- probed with several PT100
- girder is isolated by walls and ceiling to reproduce a cell of the storage ring
- fan is integrated

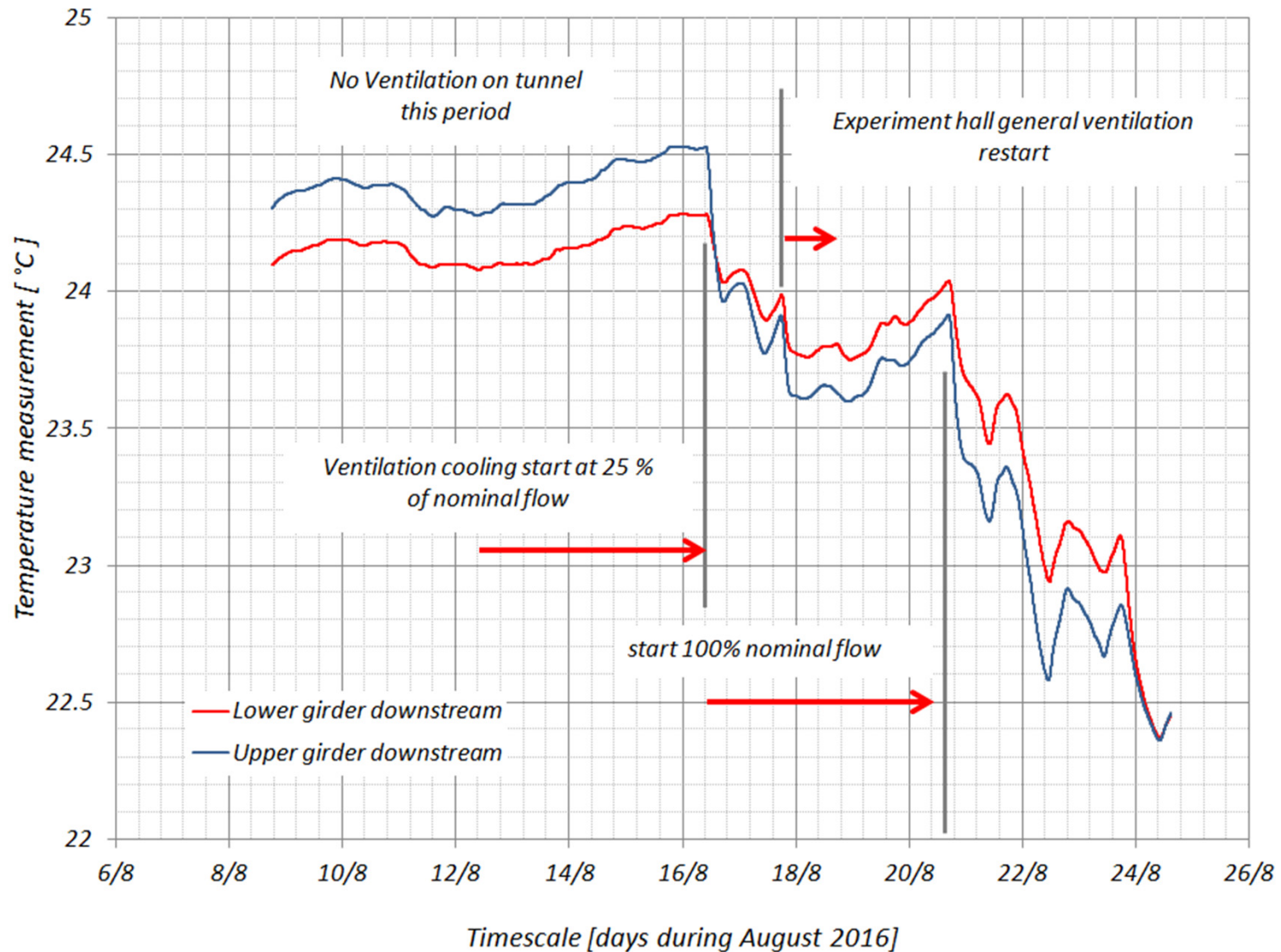


GIRDER MOCK-UP – TEMPERATURE PROBES

Power and ventilation Transient phase at Chartreuse test model



EBS girder thermal behaviour at Chartreuse test model



CONCLUSION

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THANK YOU FOR YOUR ATTENTION