

Difracción de polvo y su aplicación en metalurgia

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Experiments Division

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Aplicaciones del Sincrotrón ALBA a la Industria Metalúrgica y al tratamiento de superficies
Cerdanyola del Vallès, June 1st 2018

Introduction

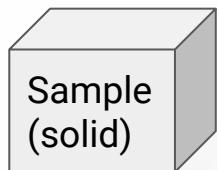
X-ray Powder Diffraction

The MSPD beamline in ALBA

Applications to Metallurgy

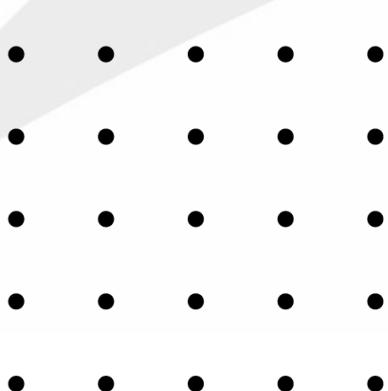
Phase analysis
Microstructure
Texture

Powder Diffraction



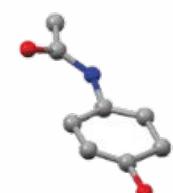
Periodical arrangement
of atoms ("crystal")

Infinite and periodic 3D arrangement of scatterers



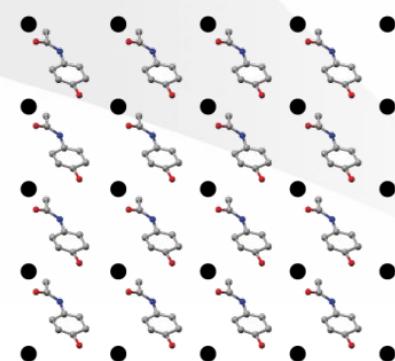
lattice

Atoms

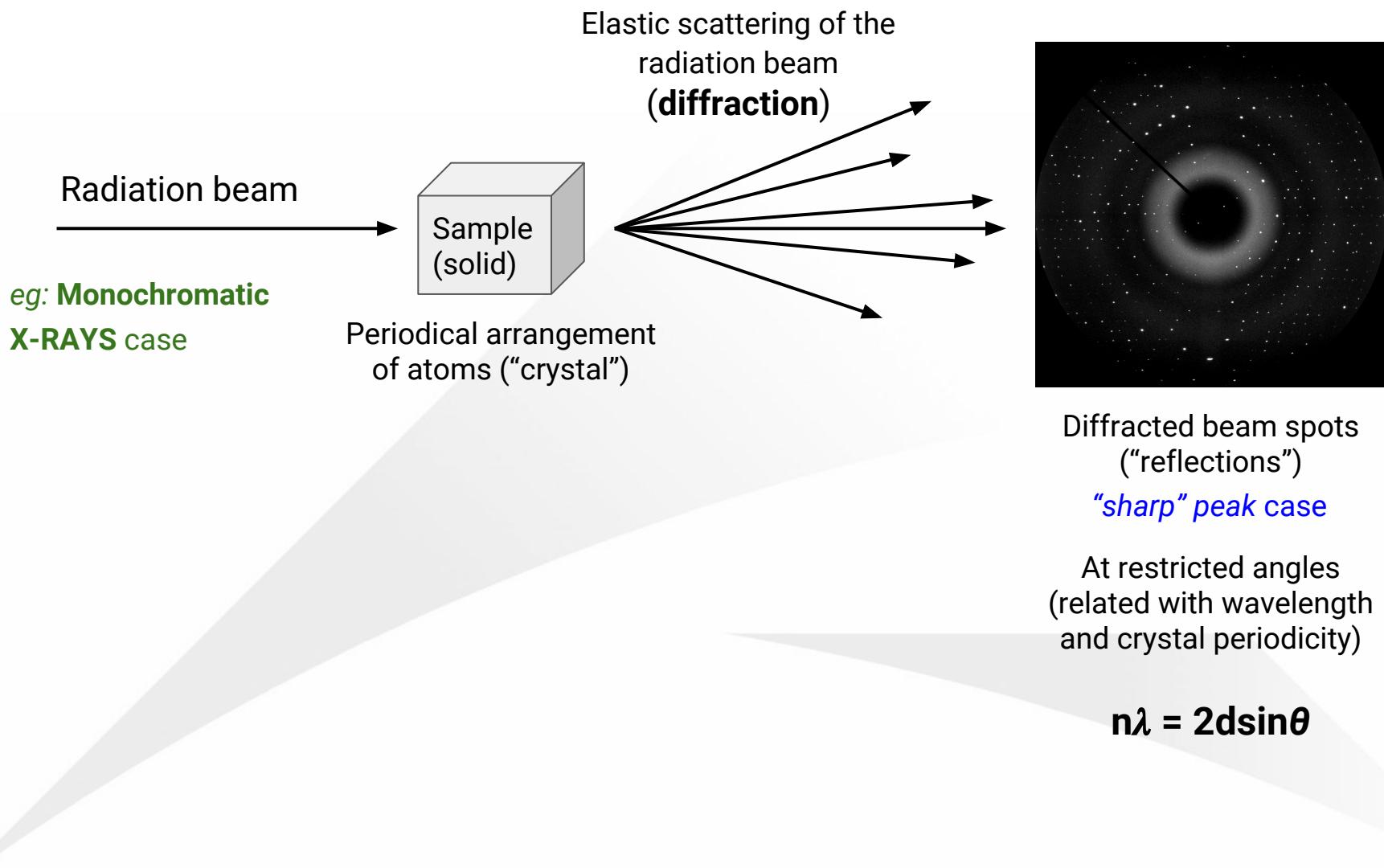


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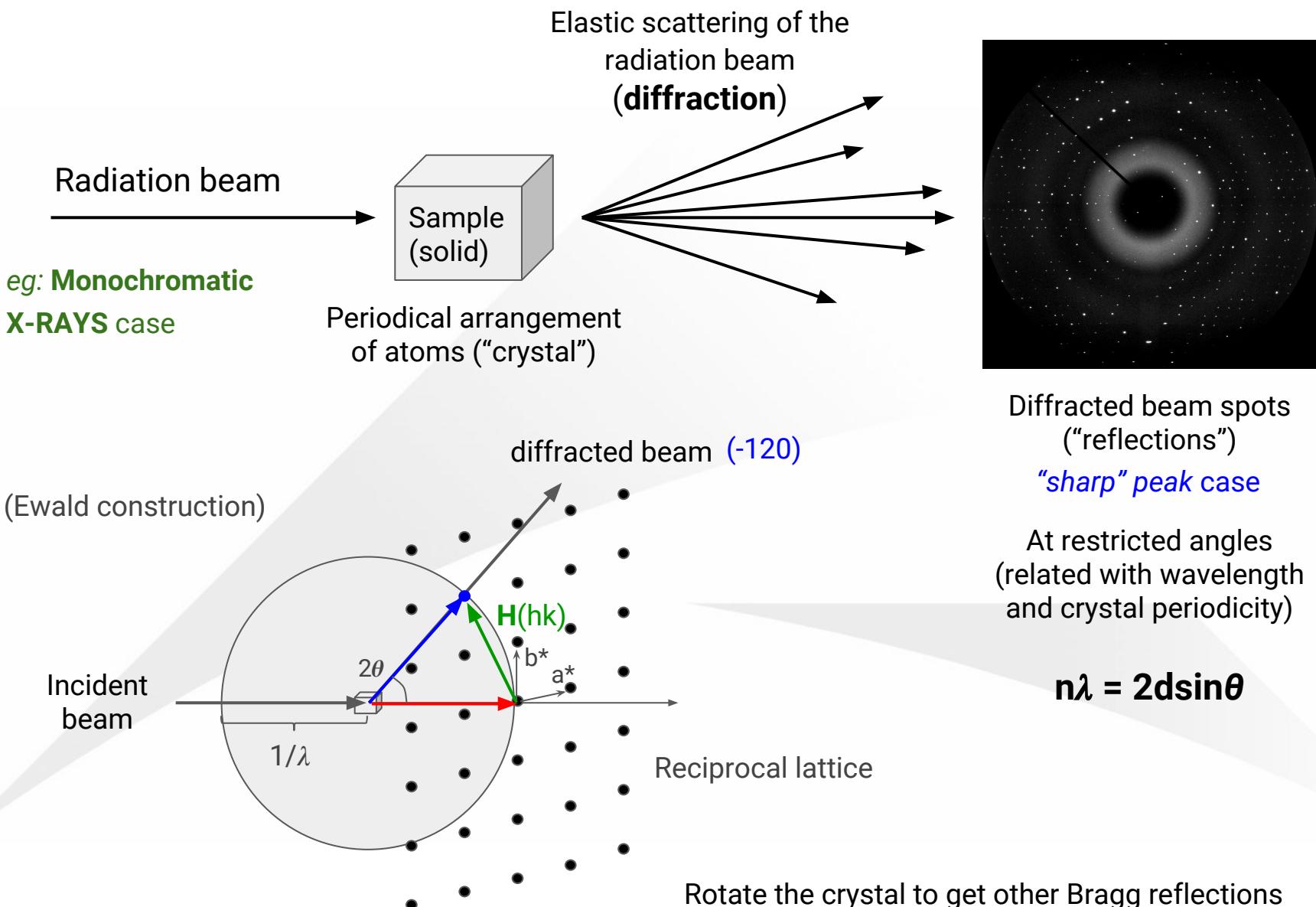
Crystal



Powder Diffraction

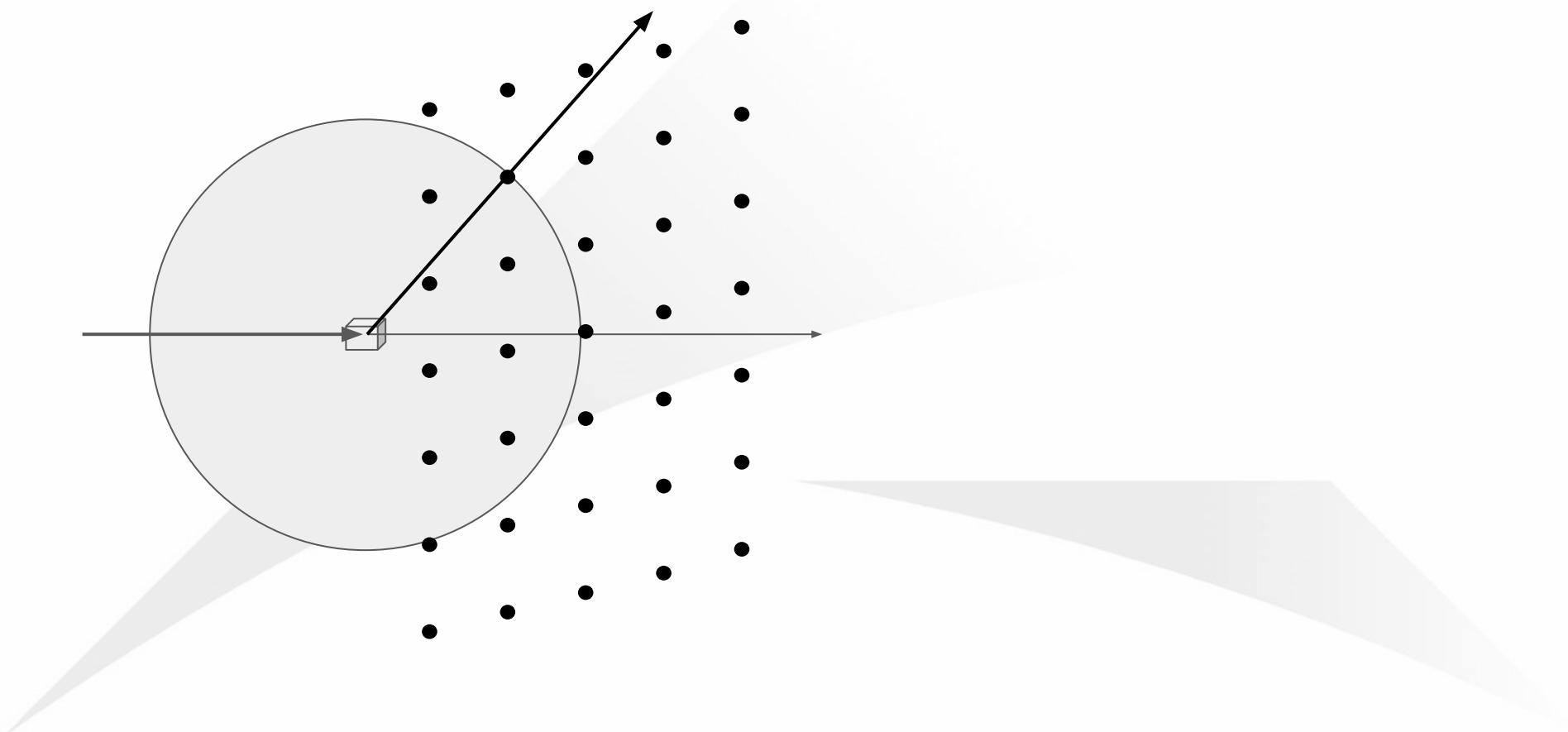


Powder Diffraction

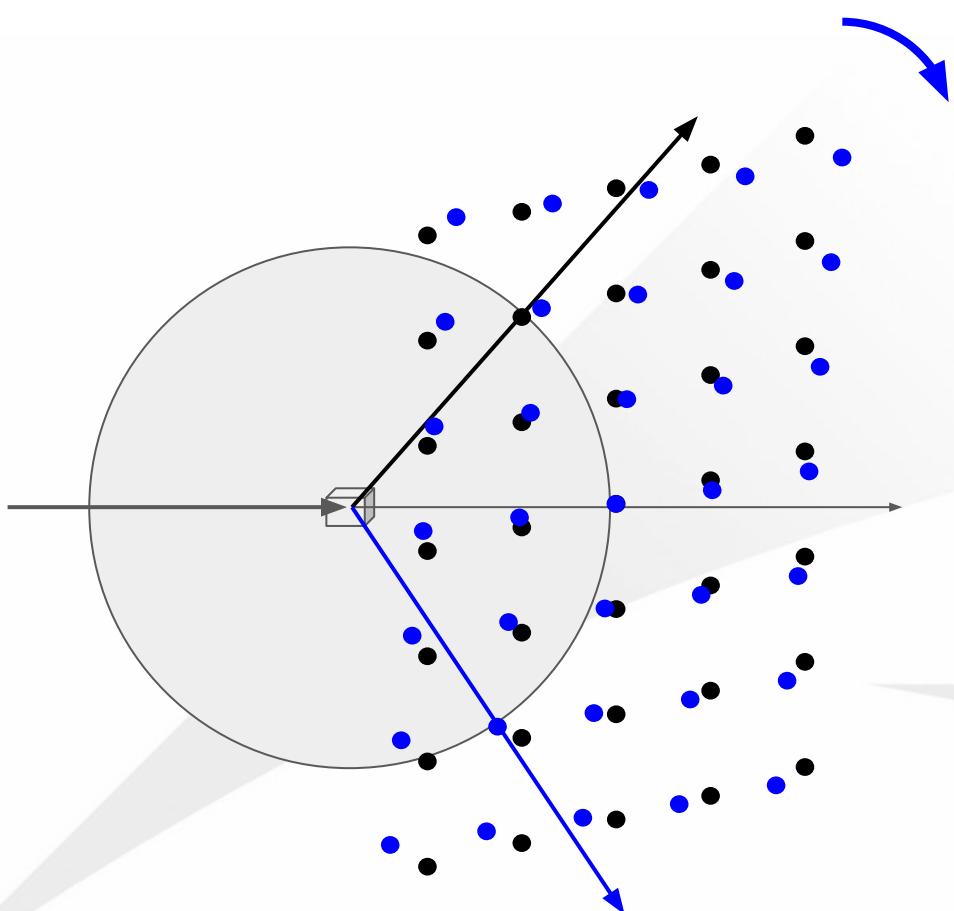


Powder Diffraction

Single crystal or “grain”

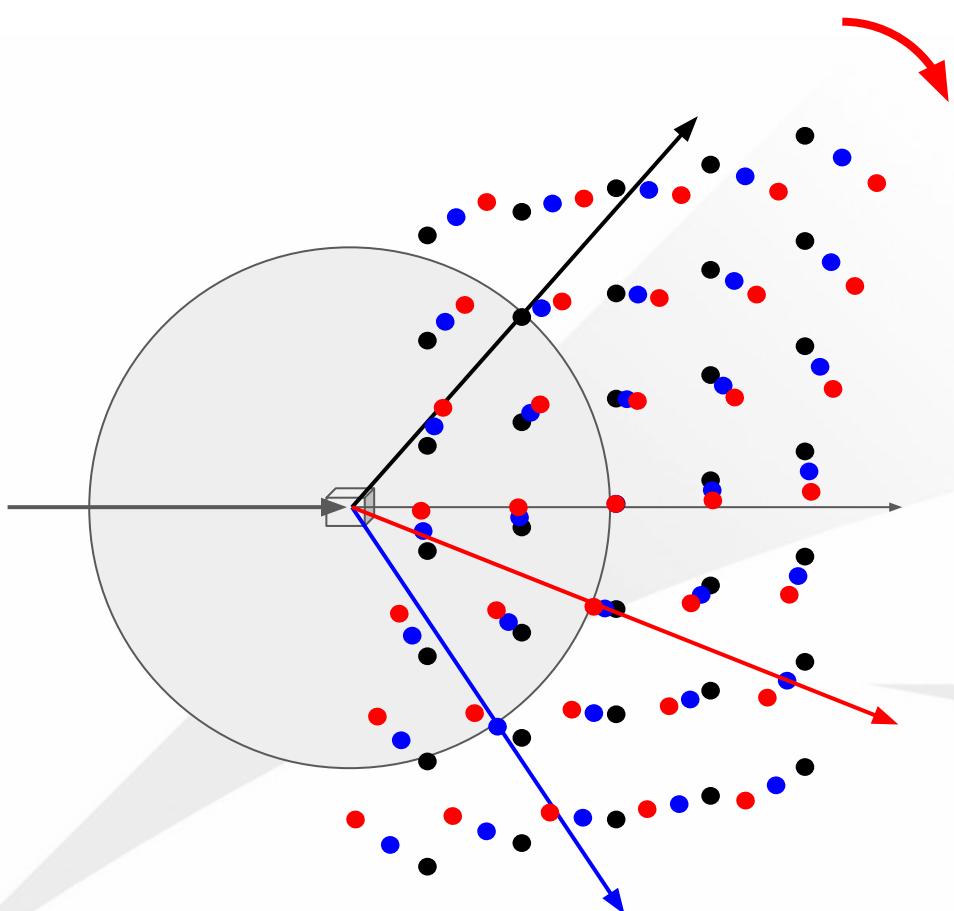


Powder Diffraction



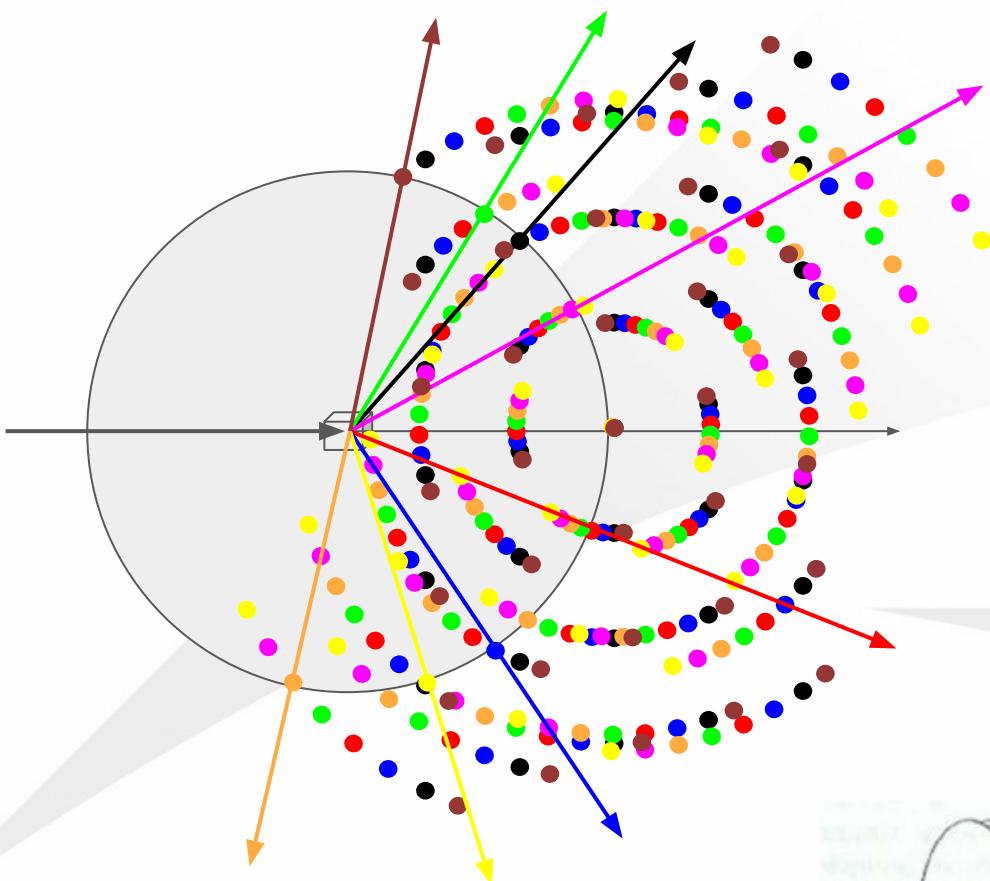
Same single crystal slightly rotated
or
2 grains with different orientations

Powder Diffraction



Same single crystal slightly rotated
or
3 grains with different orientations

Powder Diffraction

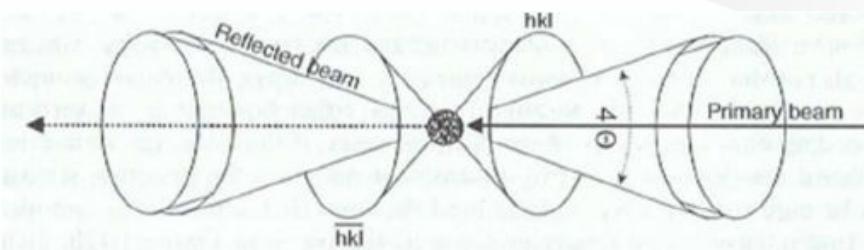


Same single crystal widely rotated
or
N grains with different orientations

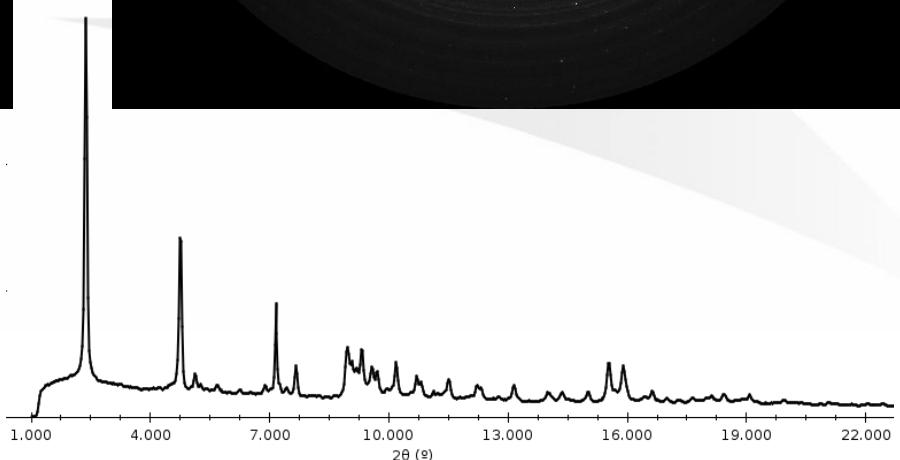
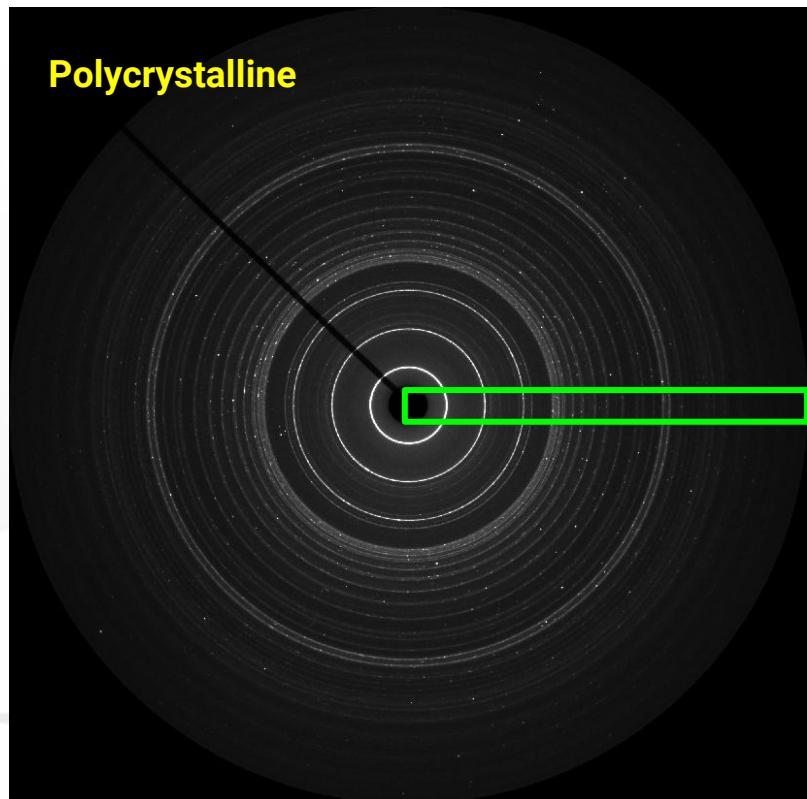
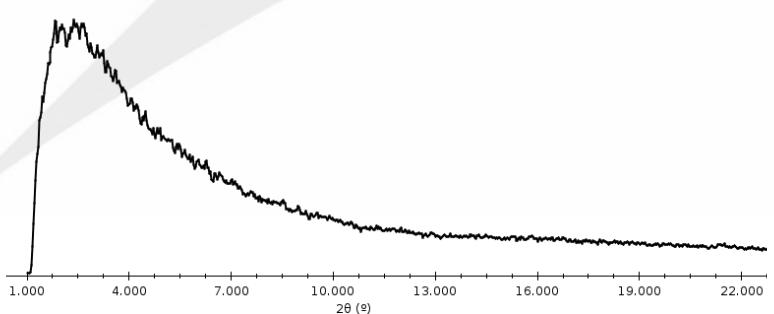
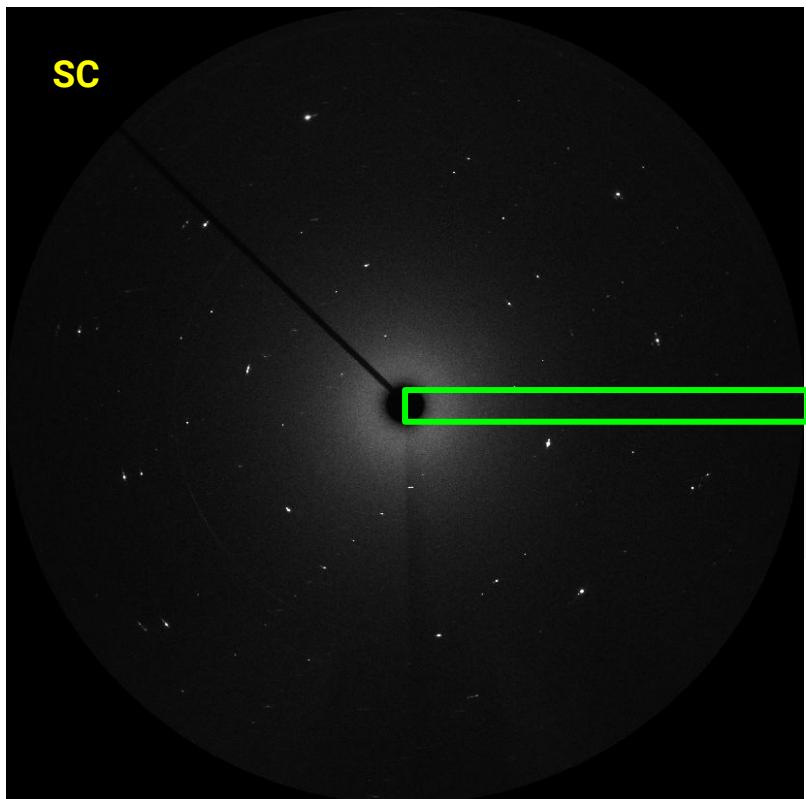
Polycrystalline diffraction (aka powder)

Diffraction is the superposition of
all the contributing crystals

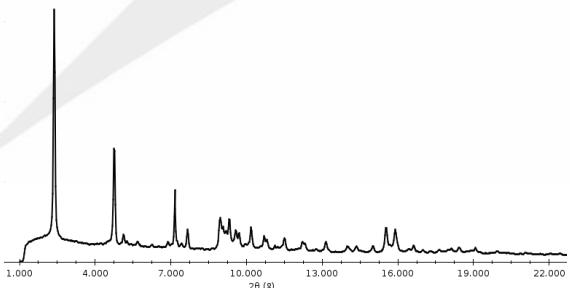
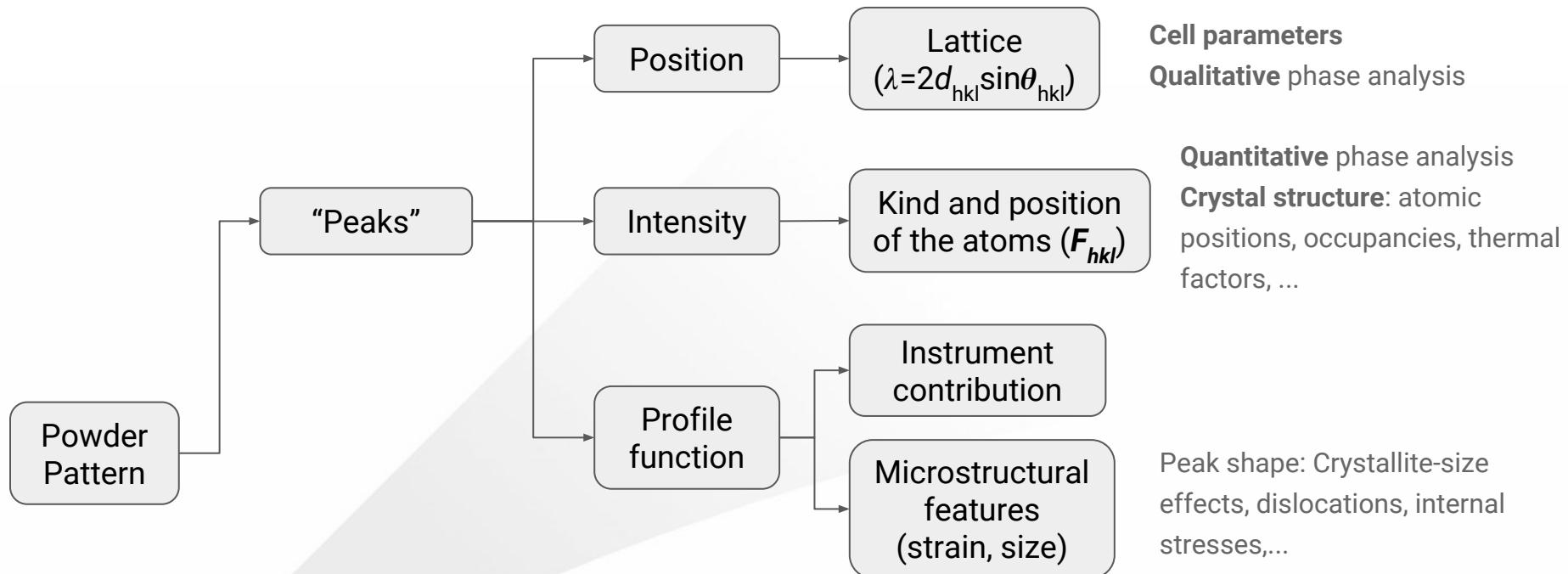
In 3D, the hkl Bragg peak is no longer
a single spot, since all same hkl spots
are at same 2θ , they lie on a **cone**
(Debye-Scherrer cone)



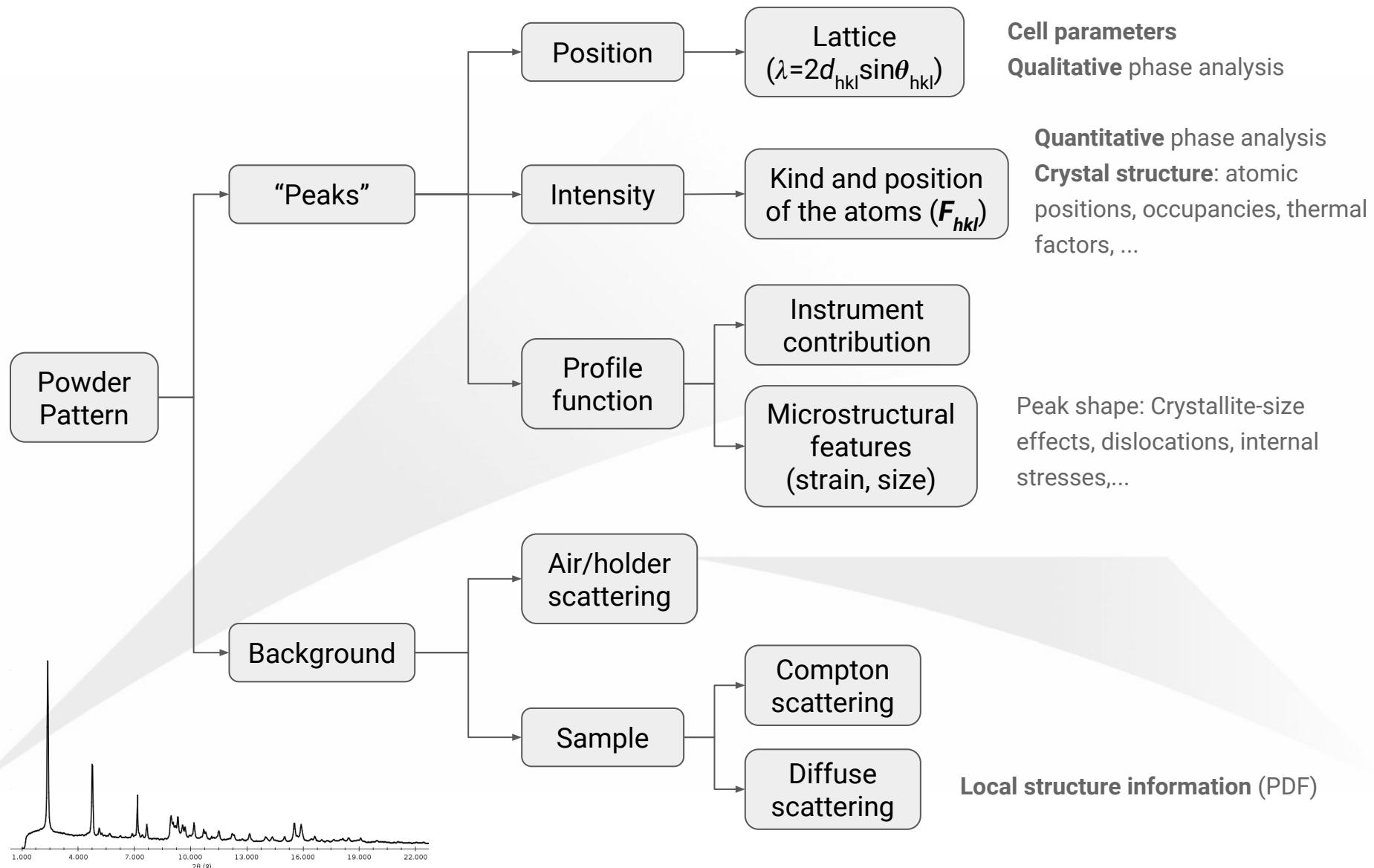
Powder Diffraction



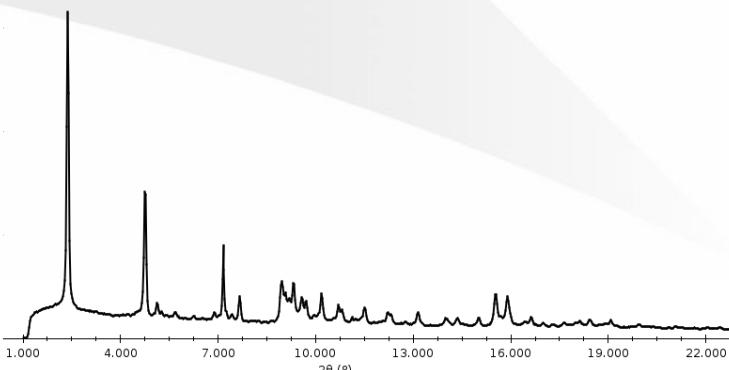
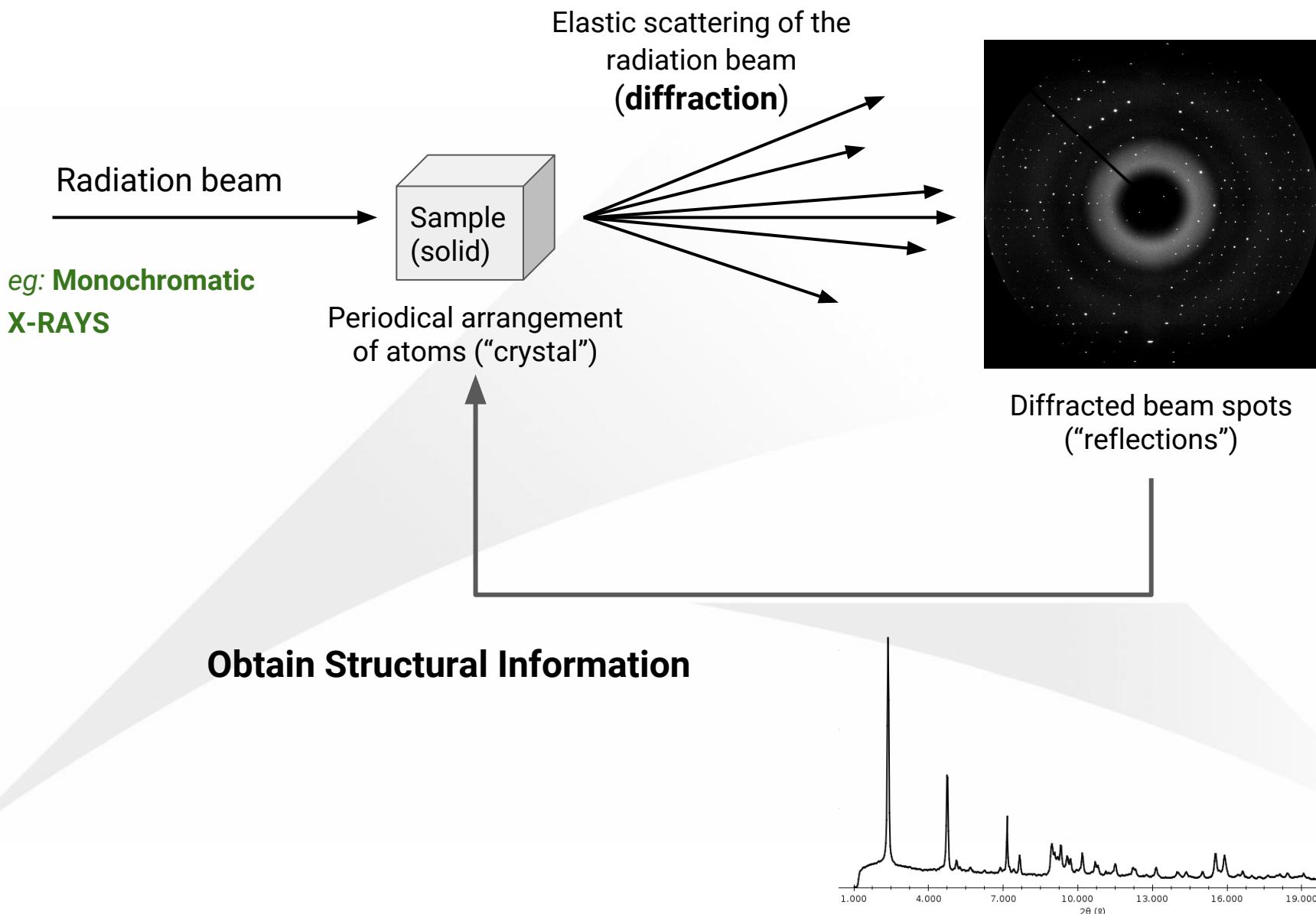
Powder Diffraction



Powder Diffraction



Powder Diffraction

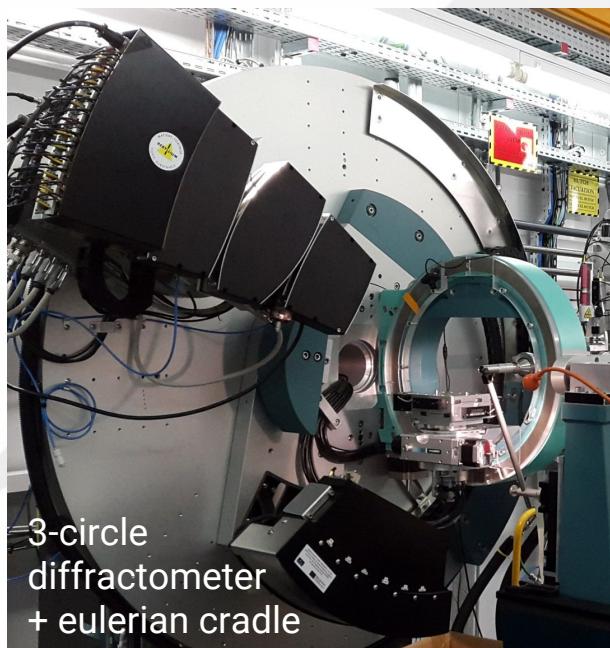


High-Resolution Powder Diffraction endstation

- Transmission measurements (capillary)
Position Sensitive (MYTHEN) or Multi-Analyzer (MAD)
- *In-situ* studies
Temperature, batteries, catalysis,...
- Other specific measurement protocols
e.g. Reflection mode (residual stress, thin films,...)

Sample Environment

- ▷ Hot air blower (300-950°C)
- ▷ LN₂ Cryostream (80-480K)
- ▷ LHe Cryostat (down to ~5K)
- ▷ Capillary flow cell
- ▷ Potentiostat
- ▷ Multispinner & coin-cell changer



Multi Analyser Detector (MAD)

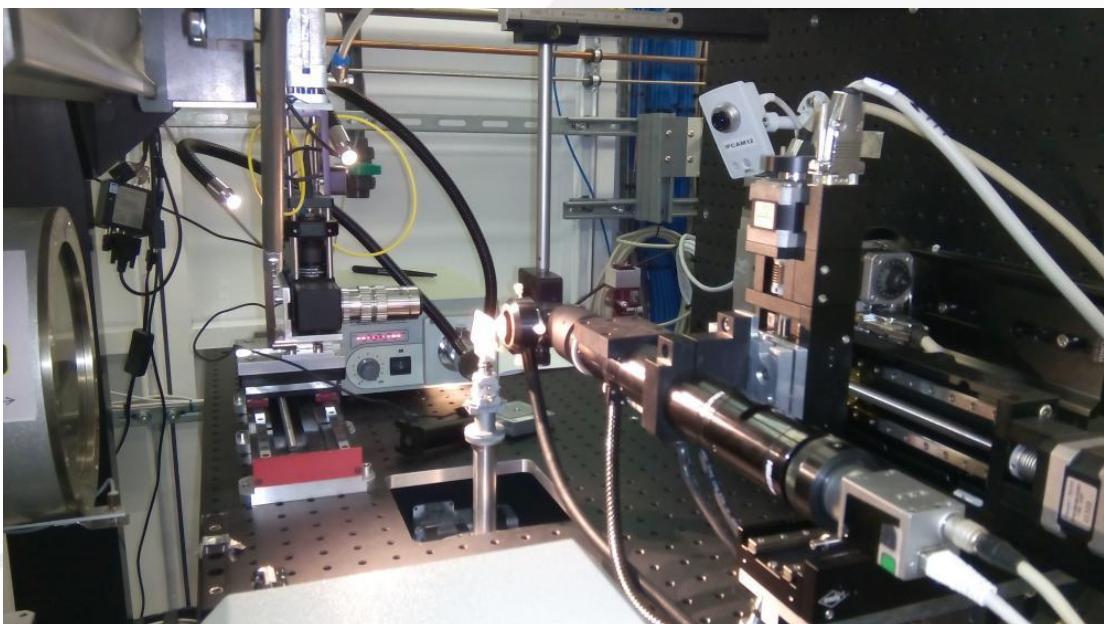
- ▷ 13 channels with 1.5° pitch
- ▷ Si111 or Si220 Bragg reflection
- ▷ YAP scintillator + PMT
- ▷ 10 to 50 keV

MYTHEN-II detector

- ▷ 6 modules (1280 channels, 50µm pitch)
- ▷ Sample to Det. dist. 550mm (40° 2θ in 0.005° pitch)
- ▷ ms time resolution
- ▷ 7 to 30 keV
- ▷ Up to Q~27 Å⁻¹ for total scattering exps. (120°/30keV)

High-Pressure/μXRD endstation

- High-pressure experiments (DACs)
- Microdiffraction
 - Free-standing, sc, cultural heritage, texture,...
- Other specific measurement protocols
 - e.g. Non-KB, reflection, capillary cells, ...



Kirkpatrick-Baez (KB) focusing optics

- ▷ Spot size of 15 x 15µm FWHM at sample position (20-50 keV)

Sample mounting/environment

- ▷ XYZ stage, omega (and chi)
- ▷ Diamond anvil cells (+ temperature)
- ▷ Spectrometer for online pressure calibration (Ruby)
- ▷ Online visualization system

CCD camera

- ▷ SX165 (Rayonix)
- ▷ Round area (Ø165mm)
- ▷ 20 to 50 keV
- ▷ Dynamic range 16 bit

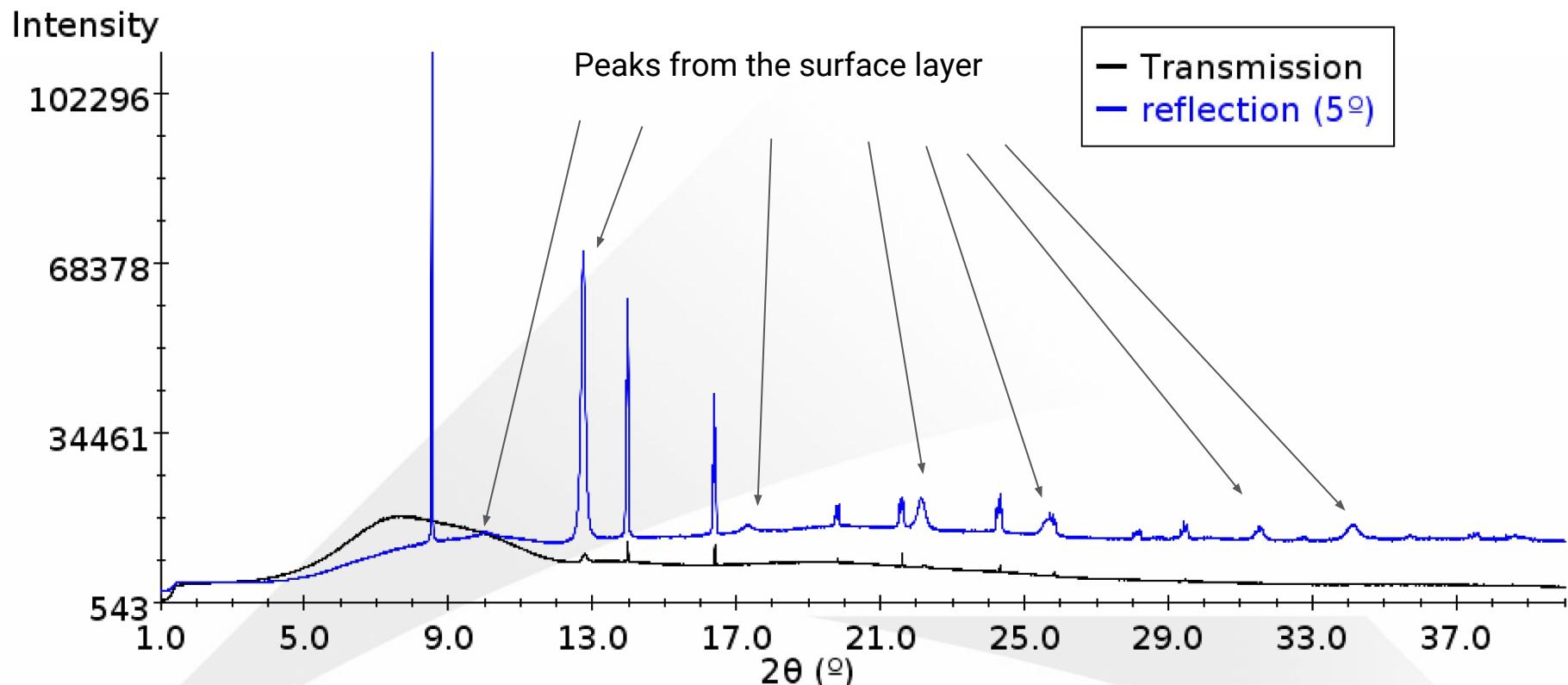
Synchrotron X-ray diffraction advantages

High flux
Broad range of energies
Low natural beam divergence
Small spot size
Detector systems
Sample environments

Radiation damage
Grain size / Homogeneity
(powder diffraction)

Penetration of absorbing materials
Fast acquisitions (Time-resolved studies)
Good signal to noise, statistics
High angular resolution
Small amount of sample required
Measurement of small volumes
In-situ studies

Reflection experiments



- For thick samples with high absorption
- For thin layers on “substrates”
- Improve the contribution of the surface
- Qualitative analysis

Applications in metallurgy

Qualitative and Quantitative phase analysis

Crystalline phases in the material
(peak position and intensity)

Microstructure

Particle size, stress
(peak width, shape and position)

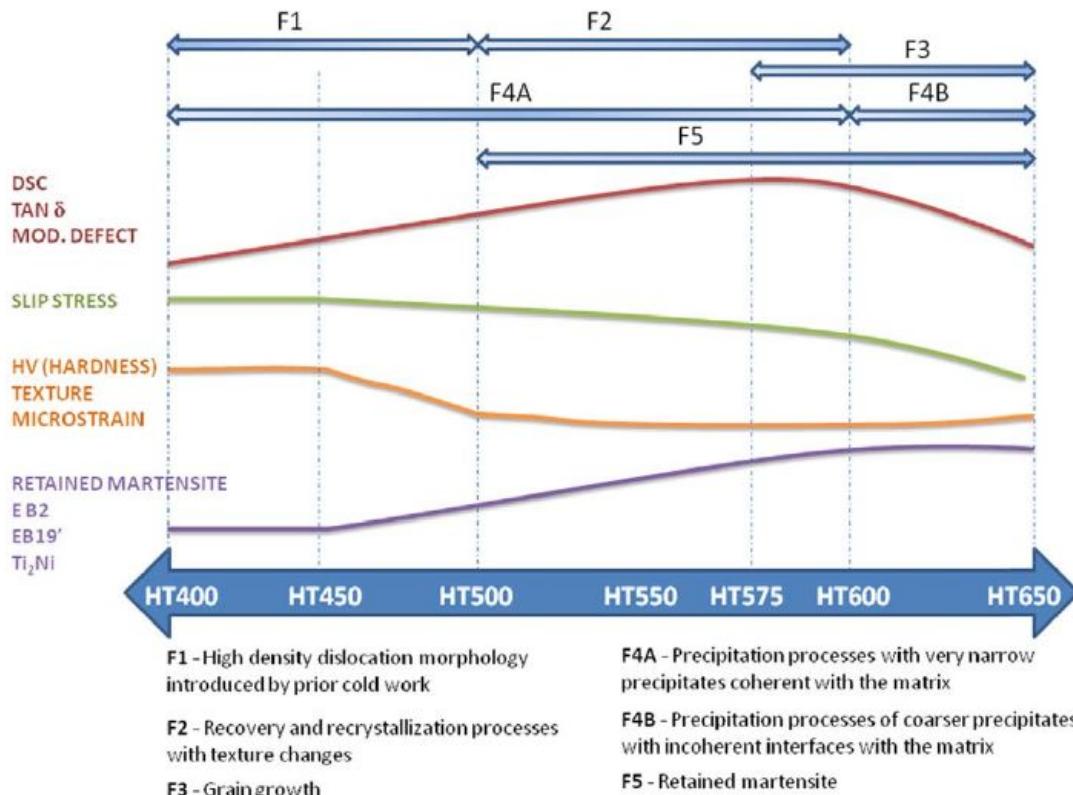
Texture

Orientation of the material
(Intensities from certain families of reflections)

(influence on material properties)

Effects of Heat-Treatment Temperature on the microstructure of the $Ti_{50}Ni_{45}Cu_5$ alloy

- Optimization of internal friction and mechanical properties by using a suitable HTT.



Summary of the tendencies of the studied properties with HTT and the correlation with the causing factors.

- PD to study changes that the HTT causes in the microstructure (crystallite size, wt% phases, microstrain and texture)

Identifying the effects of heat treatment temperatures on the $Ti_{50}Ni_{45}Cu_5$ alloy using dynamic mechanical analysis combined with microstructural analysis. A. Fabregat-Sanjuan, F. Gispert-Guirado, F. Ferrando, & S. De la Flor. *Materials Science and Engineering: A*, 2018, 712, 281–291.

Effects of Heat-Treatment Temperature on the microstructure of the $Ti_{50}Ni_{45}Cu_5$ alloy

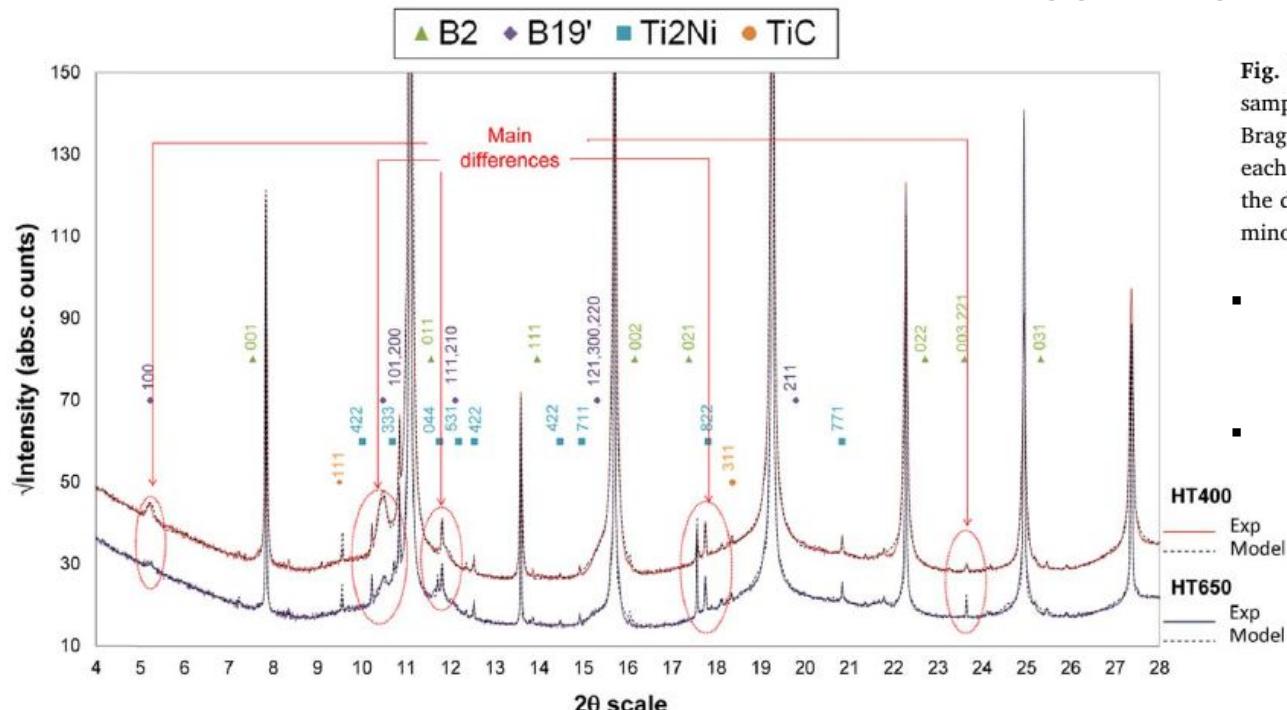


Fig. 7. Measured and calculated SXRD patterns for samples HT400 and HT650 at 120 °C. The main Bragg peaks with their hkl indexes are indicated for each phase. This plot shows the low intensity part of the diffractogram in order to reveal the peaks of the minor phases.

- Sample in **wires** measured in **transmission** (1mm diameter, 20mm length)
- **30Kev** to minimize absorption

Results of the relative quantitative analysis (in wt%) by the Rietveld method for the identified phases at 120 °C. Also shown is the conventional Rietveld agreement factor R_{wp} . n.d.: not detected.

Sample	NiTiCu-austenite (B2)	NiTiCu-martensite (B19')	Ti ₂ Ni	TiC	Cu _{0.9} TiNi _{1.1}	R_{wp}
HT400	97.65 (0.19)	1.53 (0.18)	0.53 (0.03)	0.29 (0.03)	n.d.	8.43
HT450	97.80 (0.17)	1.41 (0.16)	0.57 (0.03)	0.22 (0.03)	n.d.	9.42
HT500	96.23 (0.24)	2.95 (0.24)	0.56 (0.03)	0.26 (0.03)	n.d.	9.35
HT550	95.07 (0.25)	3.2 (0.25)	0.63 (0.03)	0.28 (0.03)	0.82 (0.06)	8.66
HT575	93.85 (0.27)	4.52 (0.26)	0.67 (0.03)	0.23 (0.03)	0.73 (0.06)	9.4
HT600	91.83 (0.29)	6.77 (0.28)	0.62 (0.03)	0.29 (0.03)	0.49 (0.07)	8.83
HT650	92.49 (0.29)	6.58 (0.28)	0.60 (0.03)	0.33 (0.03)	n.d.	9.61

Effects of Heat-Treatment Temperature on the microstructure of the $Ti_{50}Ni_{45}Cu_5$ alloy

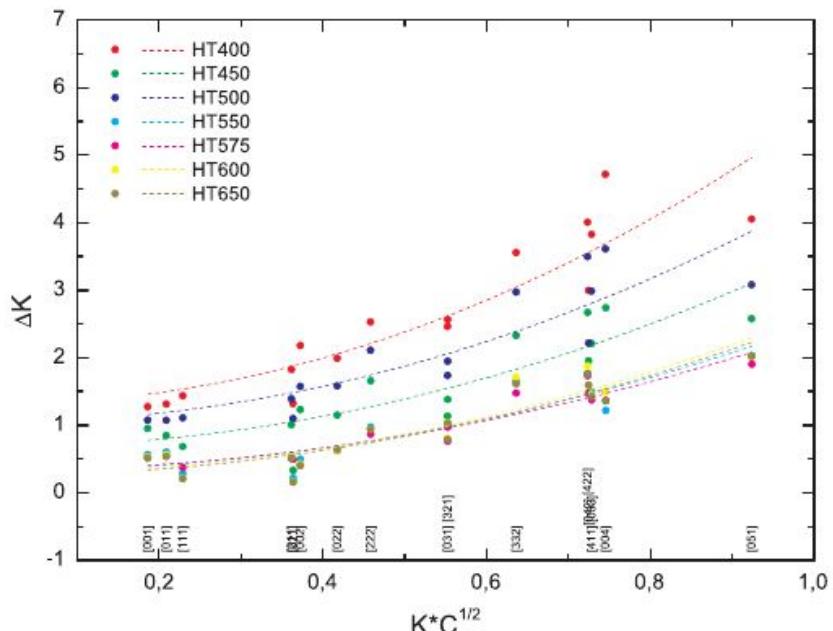


Fig. 8. Modified Williamson-Hall plot (dots) of the NiTi-austenite peaks measured at 120 °C for different temperatures of training: peak width (ΔK) v. peak position corrected by the average diffraction contrast factor ($K^*C^{1/2}$). Dashed lines: fitted function in Eq. (1) from the dots. The Miller indexes (hkl) for each peak are indicated.

Table 4

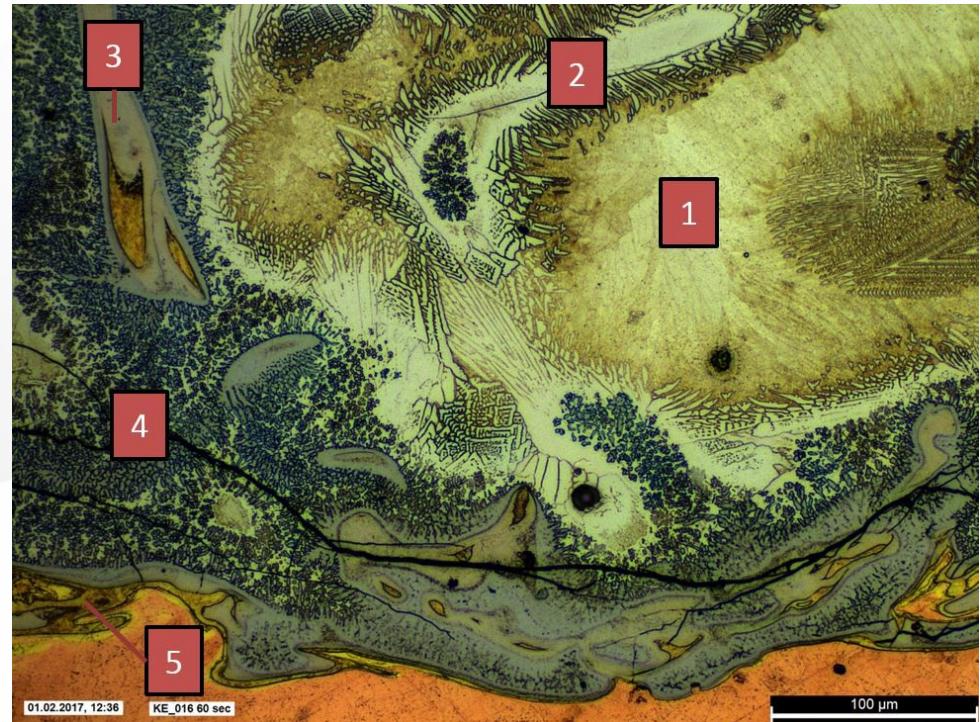
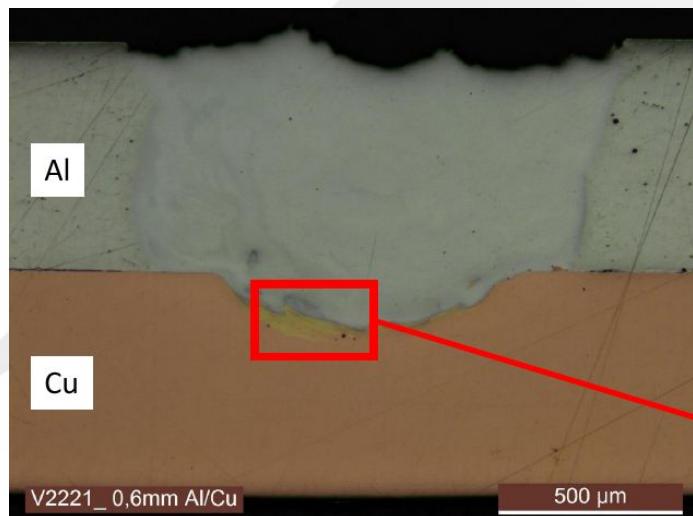
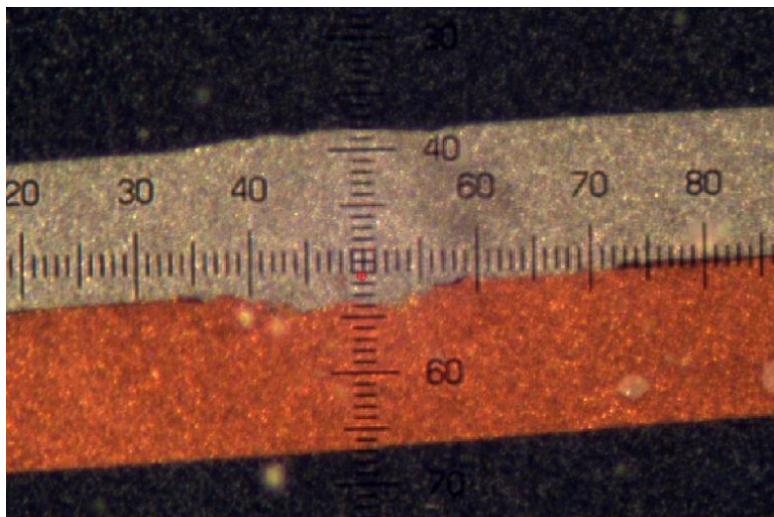
Results of the texture index calculated from the preferred orientation correction by using the general spherical harmonics correction, apparent crystallite size (D_{hkl} , in nm), density of dislocations (α') calculated with the modified Williamson-Hall plot (Fig. 8) for the NiTiCu-austenite phase, and the March-Dollase index for preferred orientation correction for NiTiCu-martensite phases and precipitates at 120 °C.

Sample at 120 °C	NiTiCu-austenite (B2)			NiTi-martensite (B19')	
	Texture index	D_{hkl}	α'	March-Dollase index	D_{hkl}
HT400	1.145 (0.002)	39 (5)	4.3 (0.5)	1.19(0.06); 0.2(0.1)	6.4(0.3)
HT450	1.113 (0.002)	76 (6)	2.8 (0.4)	1.3(0.1); 0.2(0.2)	6.3(0.4)
HT500	1.139 (0.002)	49 (10)	3.3 (0.5)	1.6(0.1); 0.2(0.2)	6.4(0.4)
HT550	1.033 (0.001)	161 (17)	2.2 (0.3)	1.5(0.2); 0.2(0.4)	6.4(0.8)
HT575	1.023 (0.001)	156 (16)	2.1 (0.2)	1.2(0.2); 0.2(0.4)	6.4(0.8)
HT600	1.024 (0.001)	191 (20)	2.4 (0.3)	1.7(0.2); 0.2(0.3)	8.2(0.8)
HT650	1.030 (0.001)	206 (23)	2.3 (0.2)	1.4(0.1); 0.2(0.9)	12.7(2.0)

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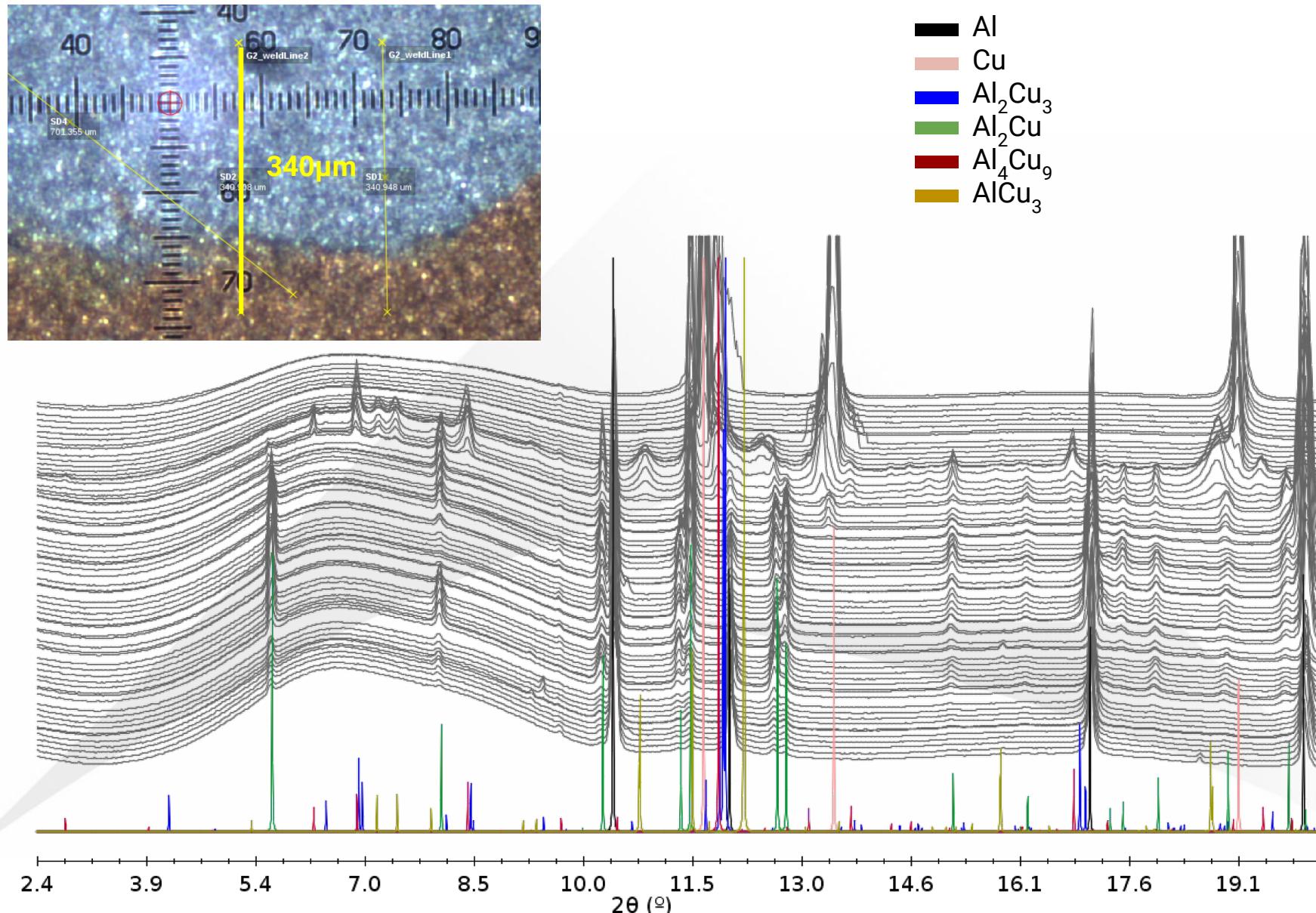
Intermetallic phases in Al-Cu joints

- Identify the IMC phases formed in the laser braze-welding process at different conditions to optimize the process parameters.



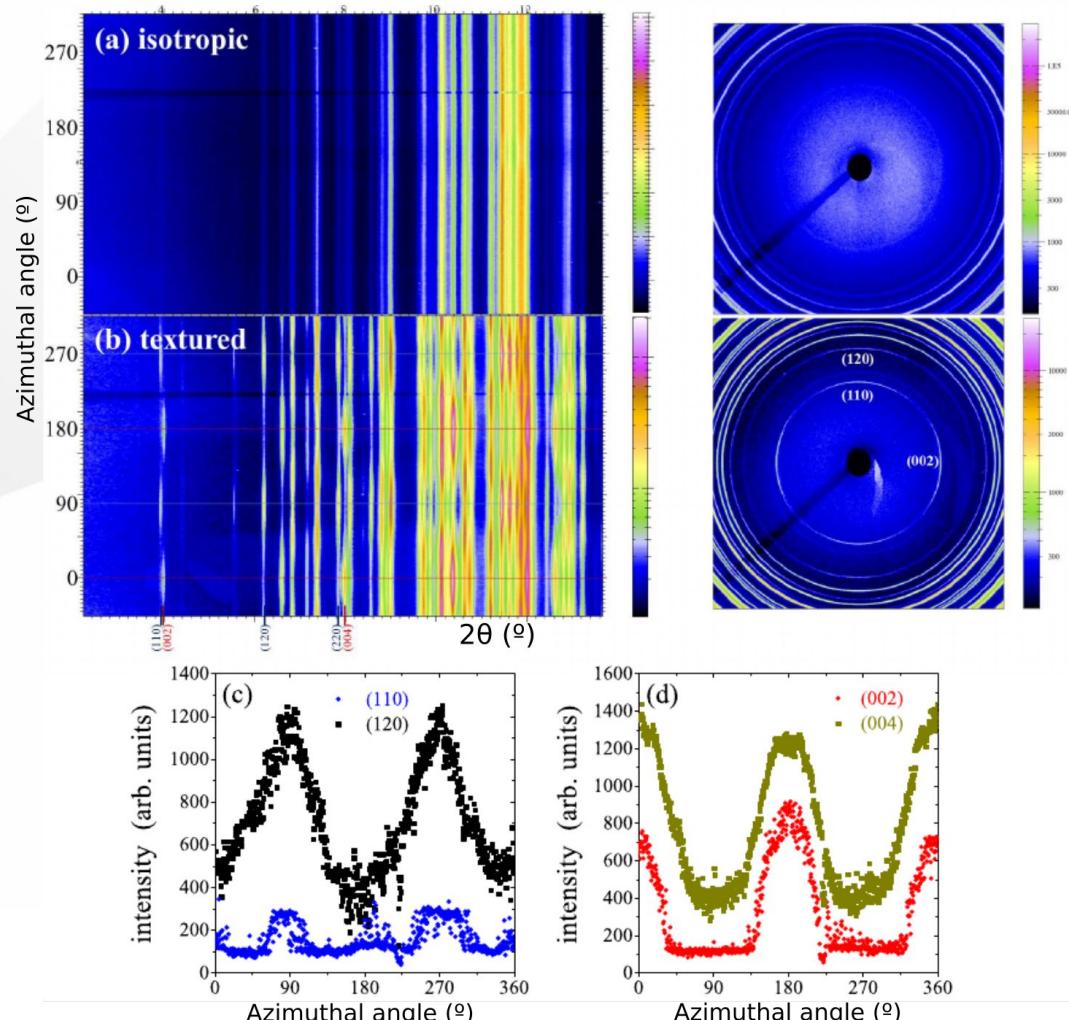
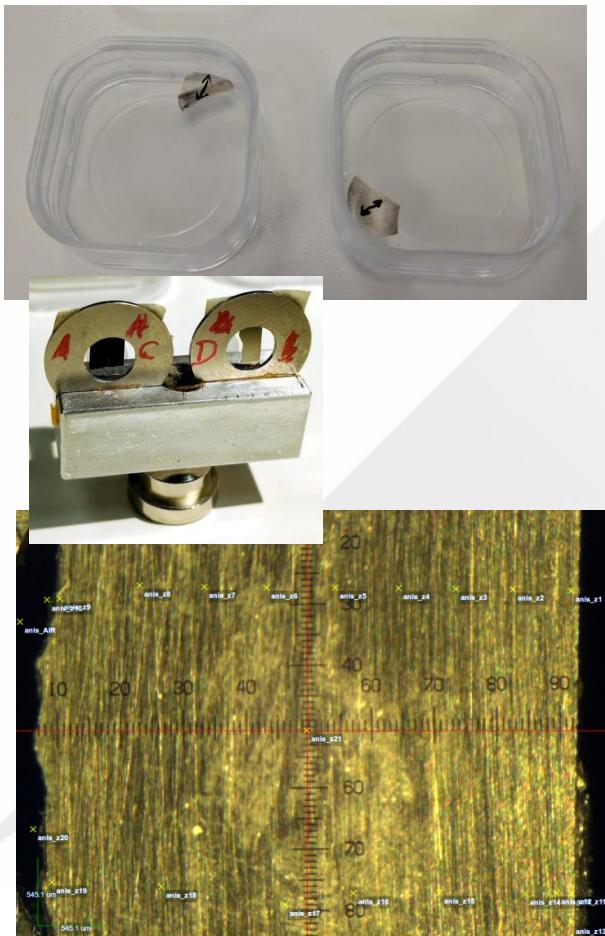
Series of measurements with a small beam size (15x15 μm) through the welding joint (transmission)

Intermetallic phases in Al-Cu joints



Texture study on Nd-Fe-B based nanocomposites

- Measurement in **transmission** to get information on the desired crystallographic axes
- 2D detector for direct texture analysis.



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Acknowledgements

MSPD Beamline team

ALBA industrial office

Thank you for your attention!



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