

High Resolution Scintillating Screens for Measurements of few Micrometer Beams

Gero Kube
DESY (Hamburg)

- Introduction
- Spatial Resolution for different Scintillators
- Influence on Observation Geometry
- Measurement of few Micrometer Beam
- Scintillator Non-Linearity
- (Comments on Digital Camera Systems)

OTR Transverse Beam Profiling

Optical Transition Radiation (OTR) for beam diagnostics

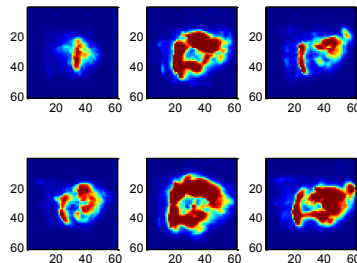
- backward OTR: reflection of virtual photons
 - instantaneous process
- single shot measurement
- full transverse (2D) profile information

Coherent OTR observation at LCLS (SLAC)

R. Akre et al., Phys. Rev. ST Accel. Beams **11** (2008) 030703

H. Loos et al., Proc. FEL 2008, Gyeongju, Korea, p.485.

➤ OTR 12



➤ OTR 22



measured spot is no beam image!

- strong shot-to-shot fluctuations
- doughnut structure
- change of spectral contents

interpretation of coherent formation in terms of “Microbunching Instability”

E.L. Saldin et al., NIM **A483** (2002) 516

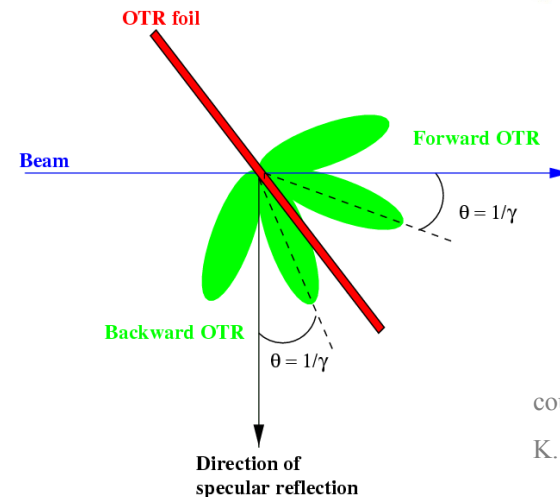
Z. Huang and K. Kim, Phys. Rev. ST Accel. Beams **5** (2002) 074401

alternative schemes for beam profile diagnostics

- stochastic radiation emission (destruction of coherence)



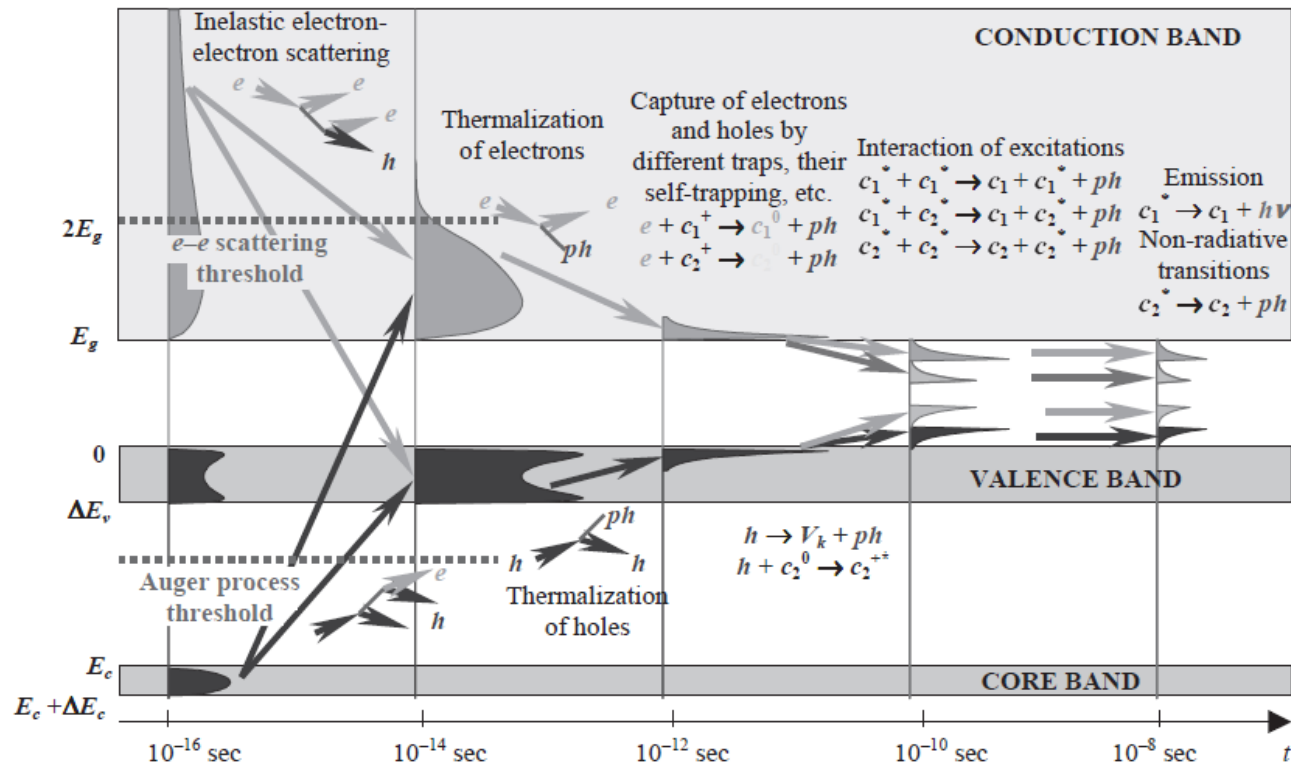
multi-stage emission process



courtesy:

K. Honkavaara (DESY)

Scintillation Light Generation



A.N. Vasil'ev, Proc. SCINT'99,
Moscow (Russia), 1999, p.43

multi-stage process

- › energy conversion → generation of “hot” electronic excitations
- › thermalization → phonon emission: transform E_{kin} of excitations in heat
- › localization → excitation interaction with defects/impurities
- › transfer to luminescent centers → migration of relaxed excitons
- › radiative relaxation → emission of scintillation light

Scintillators for Beam Diagnostics

● review of scintillators for beam profile measurements

- phosphor screens: **P11** (ZnS:Ag), **P20** ([Zn,Cd]S:Ag), **P43** (Gd₂O₂S:Tb), ...
→ decay times $O(\text{ms})$, resolution limited by grain size
- ceramic screens: Chromox (Al₂O₃:Cr)
→ higher radiation hardness, better thermo-mechanical properties, lower light yield
- inorganic scintillators: CsI:Tl, **YAG:Ce** → „high resolution monitor“ W.S. Graves et al., Proc. PAC'97 (1997) 1993
→ better resolution, higher light yield than Chromox

➡ status in 2003: R. Jung et al., Proc. DIPAC2003, IT03, p. 10

● scintillators for beam diagnostics

- heavy ion accelerators → standard for beam profile measurements (typically ceramic screens)
- electron accelerators → powders/inorganic scintillators used for gun diagnostics (OTR intensity too low)
- DIPAC invited talk 2007 → E. Bravin, „High Resolution Transverse Profile Measurement“, Proc. DIPAC2007, p.1
→ scintillators for high resolution even not covered...

● COTR problem at LCLS in 2008

- return to scintillator based beam profile diagnostics @ FELs

→ Workshop on „*Scintillating Screen Applications in Beam Diagnostics*“ @ GSI, February 2011

B. Walasek-Höhne, C. Andre, P. Forck, E. Gütlich, G. Kube, P. Lecoq, and A. Reiter, IEEE Trans. Nucl. Sci. **59** (2012) 2307

Scintillators for Beam Diagnostics (2)

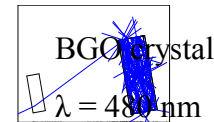
● requirements for beam diagnostics application

- high spatial resolution → material property
- high sensitivity → high stopping power, material property
- good linearity → short decay time, material property
- radiation resistant → inorganic scintillators widely used in high energy physics, dosimetry,...

unknown

● minimum distortion of optical path

- light generated inside scintillator has to cross boundary
 - refractive index n
- inorganic scintillators: **large n**
 - large contribution of total reflection
 - **influence on observation geometry**



● since beginning of 20th century: development of new inorganic scintillator materials

- high energy physics (calorimetry), medical physics (PET imaging, ...)
 - BGO, YAP, LuAG, LuAP, YAP, LSO, LYSO, GGAG, LaCl₃, LaBr₃, SrI₂, ...



interest in testing new materials for beam diagnostics (→ why only YAG:Ce ?)

Test Experiments

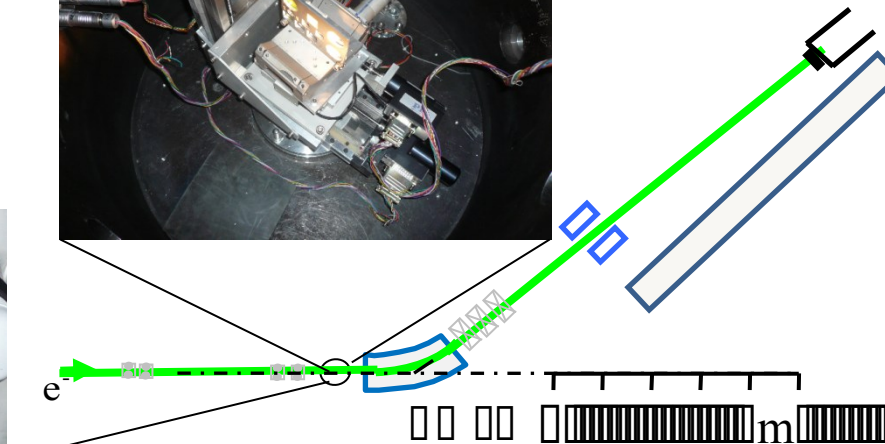
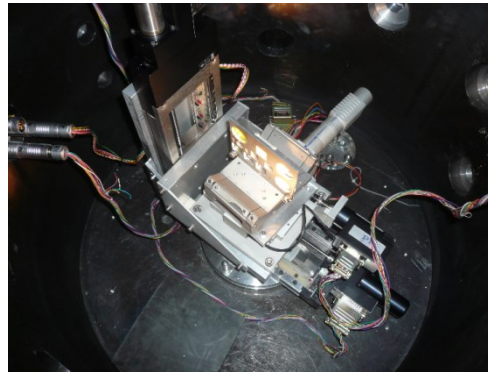
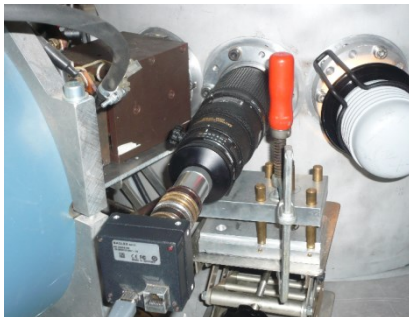
● Mainz Microtron MAMI

Institute of Nuclear Physics, University of Mainz (Germany)

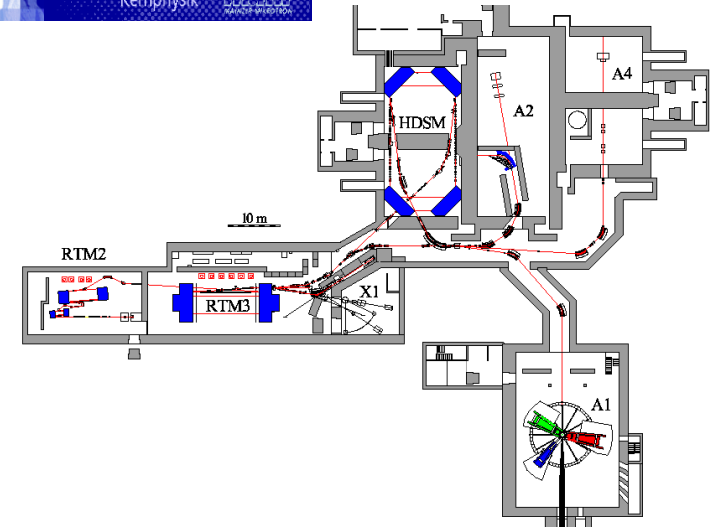
3 cascaded Racetrack Microtrons: $E_{\text{max}} = 855 \text{ MeV}$
 double-sided Microtron (HDSM): $E_{\text{max}} = 1.5 \text{ GeV}$
 100 % duty cycle
 polarized electron beam ($\sim 80\%$)

● test experiments in X1 beamline

- target chamber with goniometric stages
- observation geometry -22.5° w.r.t. beam axis



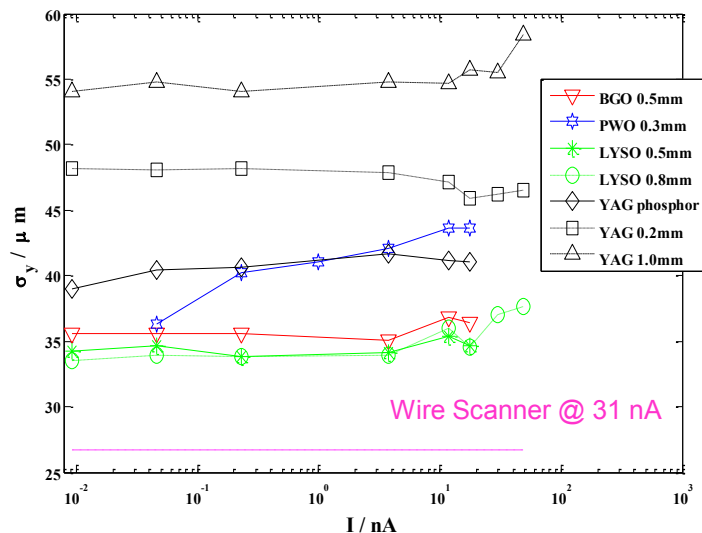
➤ target holder



Spatial Resolution

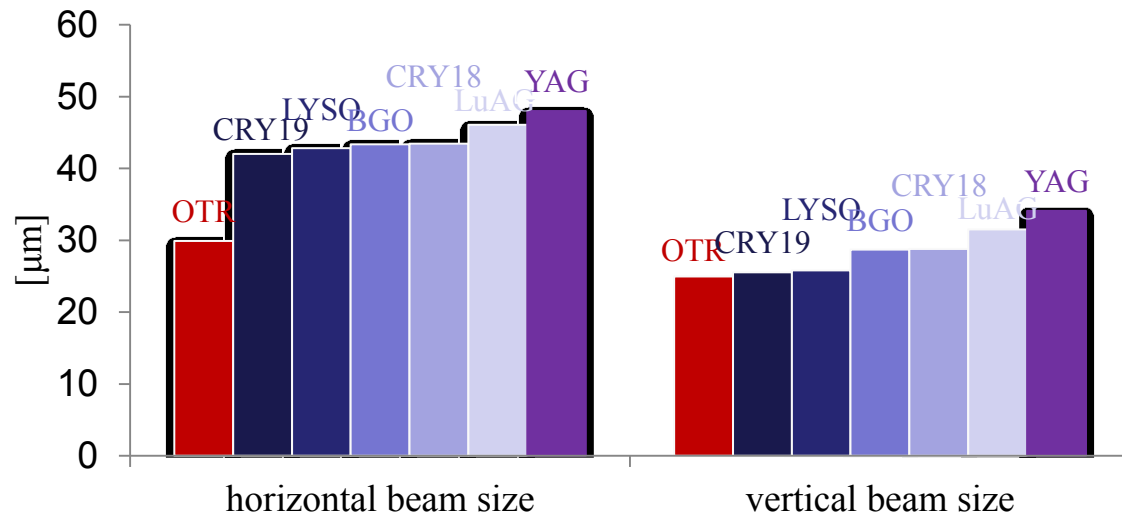
experiment 2009

- BGO 0.5 mm
- PWO 0.3 mm
- LYSO:Ce 0.8 mm, 0.5 mm (Prelude 420)
- YAG:Ce 1.0 mm, 0.2 mm, powder
- Al₂O₃ 1.0 mm (ceramic)



experiment 2011

- BGO 0.3 mm
- LYSO:Ce 0.3 mm (Prelude 420, CRY-19)
- YAG:Ce 0.3 mm
- LuAG:Ce 0.3 mm
- YSO:Ce (?) 0.3mm (CRY-18)



G. Kube et al., Proc. IPAC'10, Kyoto (Japan), 2010, p.906

G. Kube et al., Proc. IPAC'12, New Orleans (USA), 2012, p.2119



LYSO:Ce best spatial resolution

Observation Geometry

- beam diagnostics

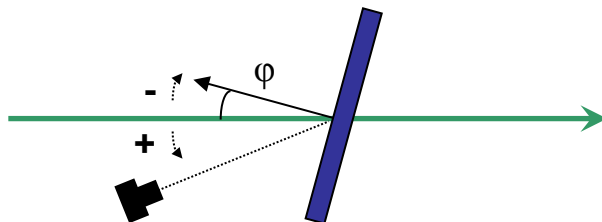
→ popular OTR-like observation geometry:

45° tilt of screen

observation under 90°

→ **turns out to be bad!**

- scintillator tilt versus beam axis

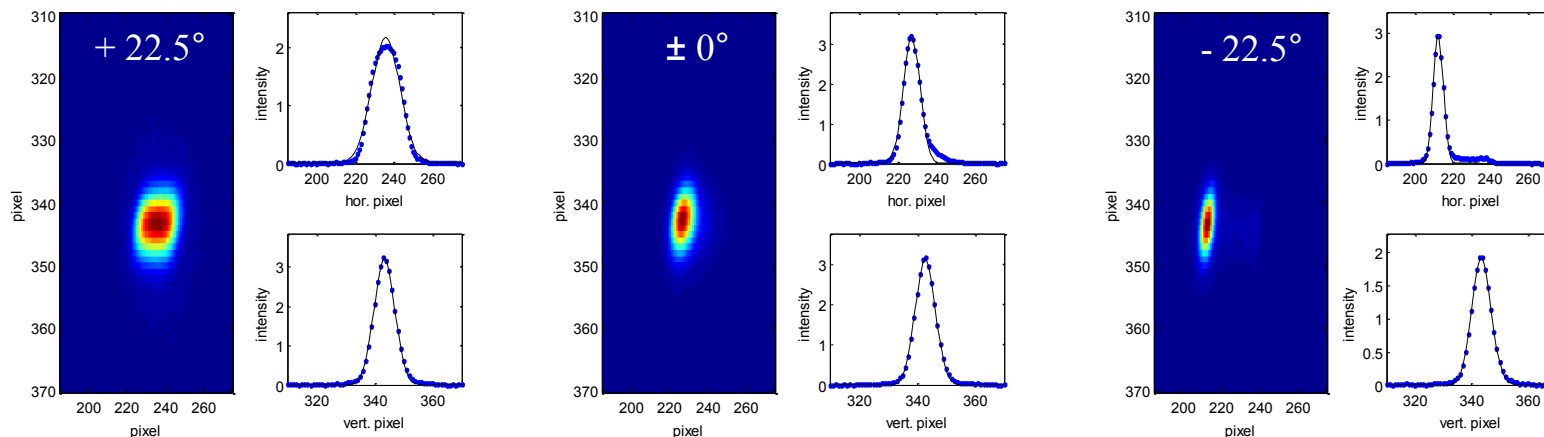


BGO crystal

micro-focused beam

$I = 3.8 \text{ nA}$

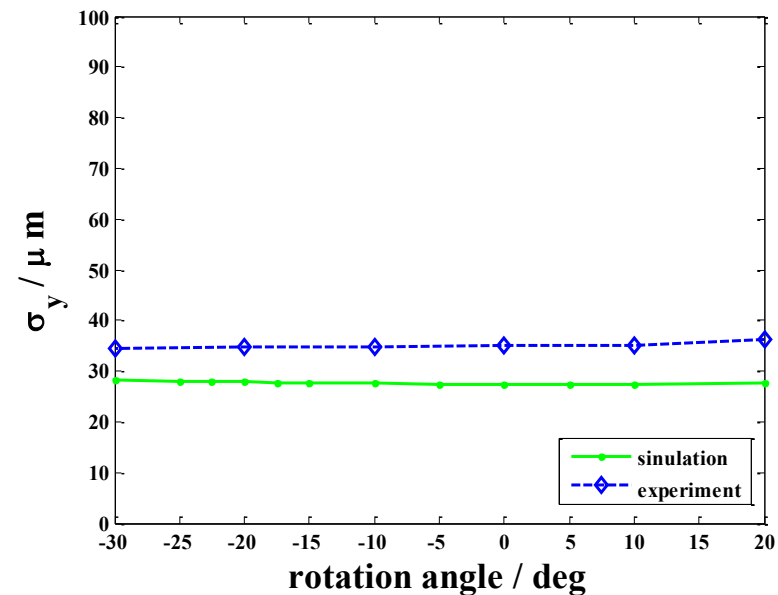
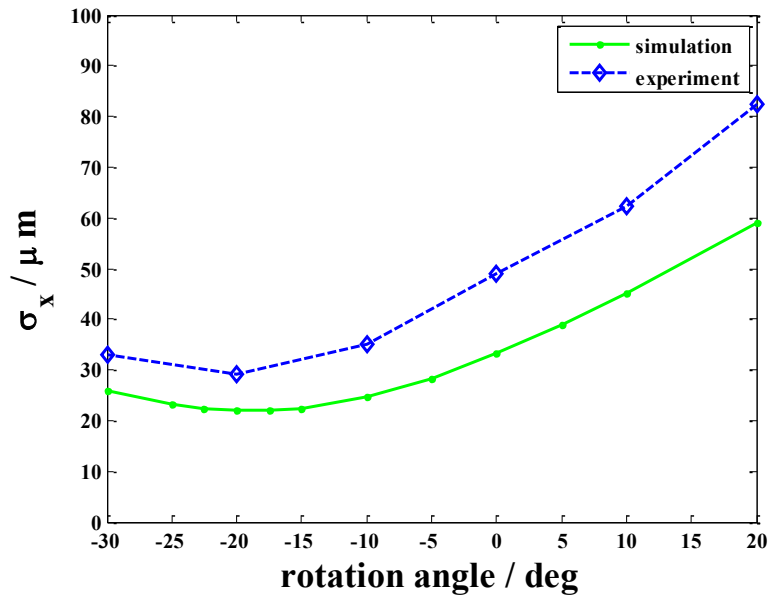
- measured beam spots



Comparison

- light propagation in scintillator

➤ simple ZEMAX model → light generated by line source, scintillator characterized by n



- satisfactory agreement between simulation and measurement

→ simulation reproduces observed trend in beam size

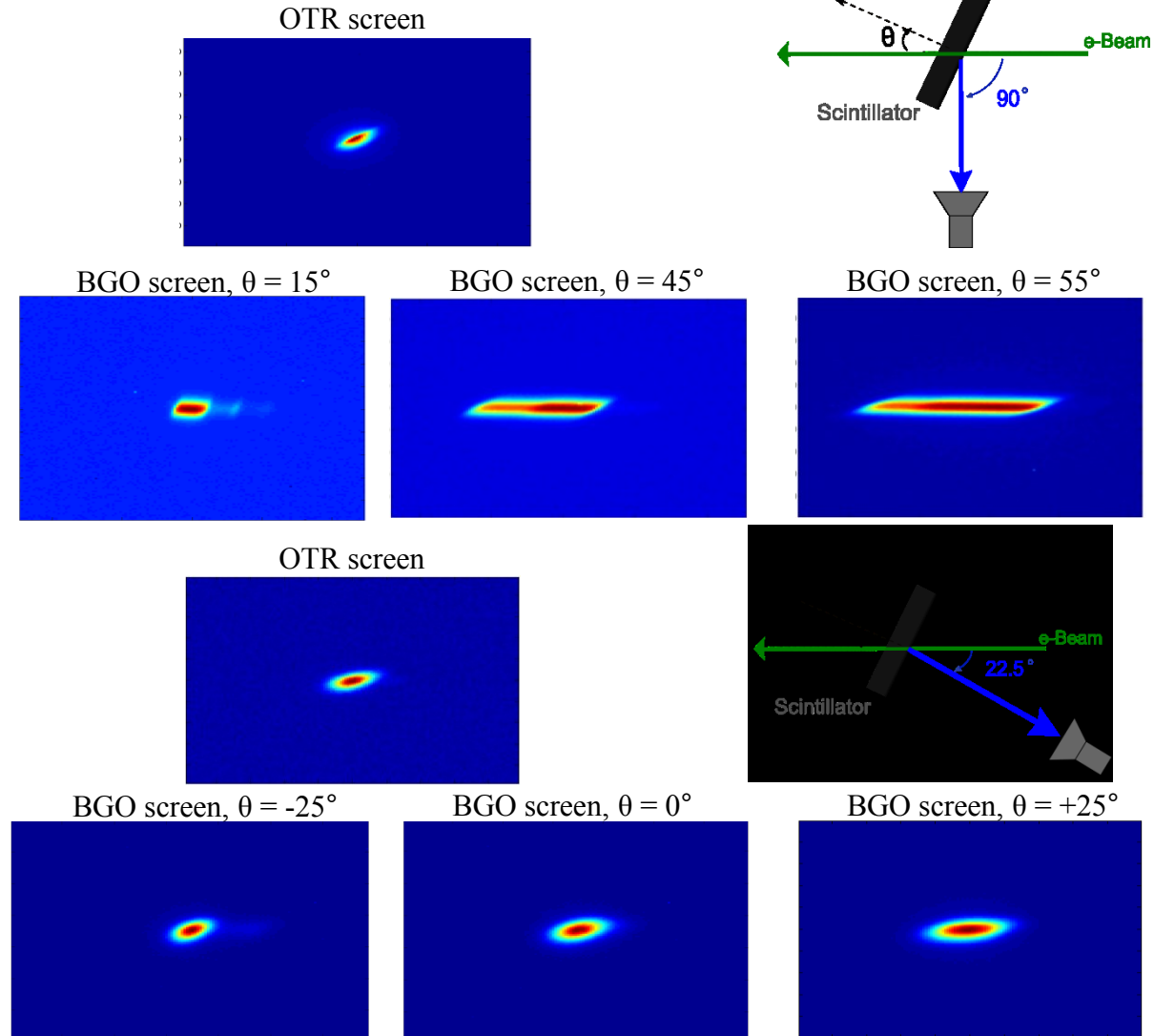
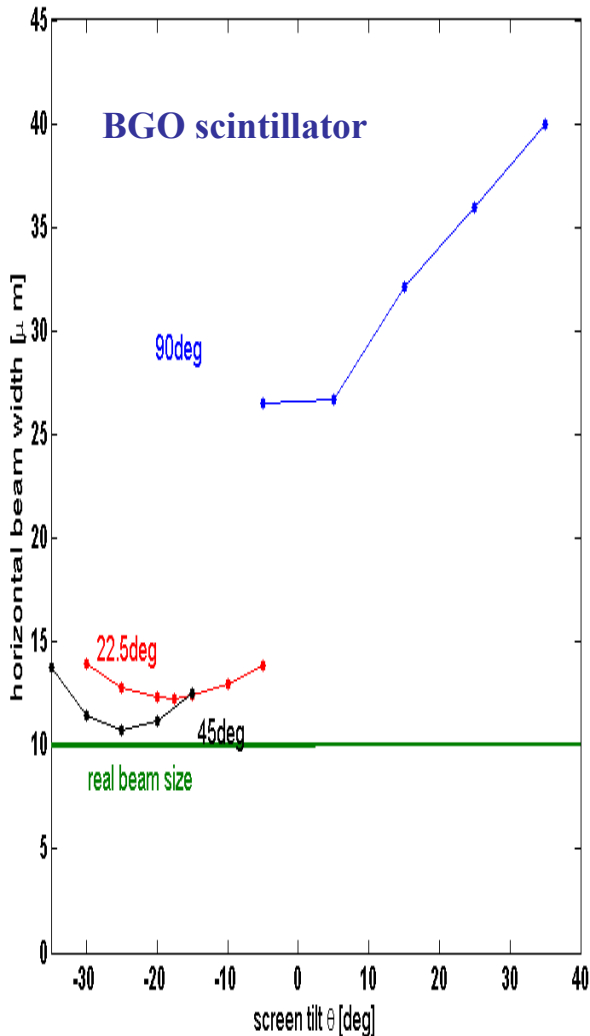
- measured beam size systematically larger than simulated one

→ effect of scintillator material properties not included in calculation → increase in PSF

G. Kube, C. Behrens, and W. Lauth, Proc. IPAC 2010, Kyoto, Japan, p.906.

Observation Geometry Influence

● comparison observation geometry

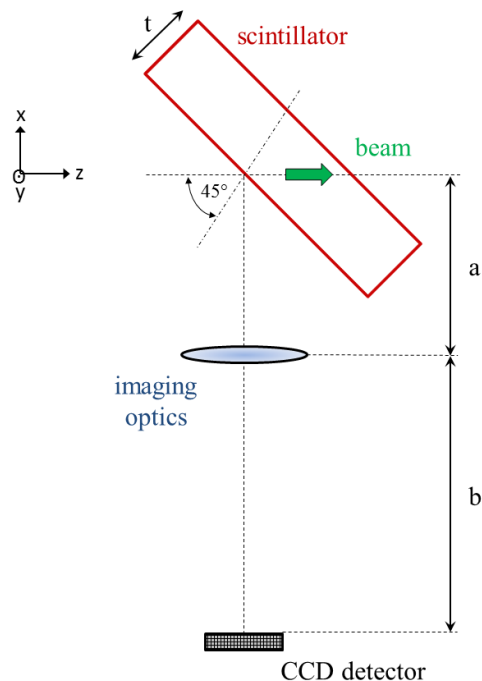


Exploring the Resolution Limits

micrometer beam size experiment at MAMI

G. Kube, S. Bajt, A.P. Potylitsyn, L.G. Sukhikh, A.V. Vukolov, I.A. Artyukov, W. Lauth, Proc. IBIC2015, Melbourne, Australia, p.330

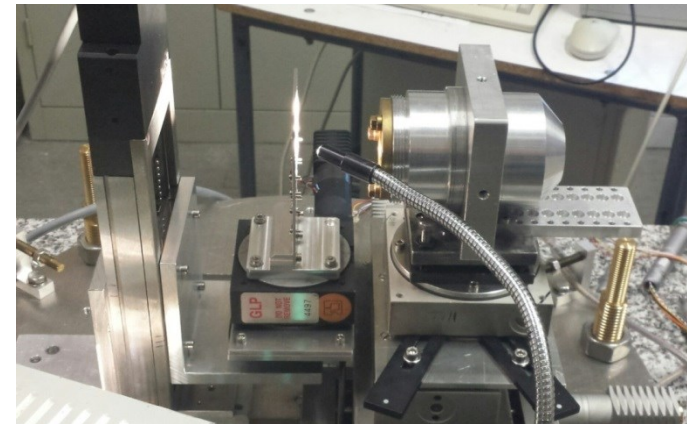
experimental scheme



$$a = 27.54 \text{ mm}$$

$$b = 1155.46 \text{ mm}$$

$$\rightarrow M = 41.95$$



Target: LYSO scintillator ($\text{Lu}_{2(1-x)}\text{Y}_{2x}\text{SiO}_5:\text{Ce}$)

thickness $t = 200 \text{ }\mu\text{m}$

supplier: *OmegaPiezo*

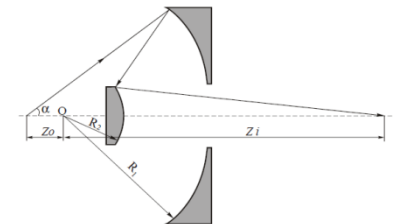
Schwarzschild Objective:

→ 2 concentric spherical mirrors

→ aplanatic (corrected for spherical aberrations)

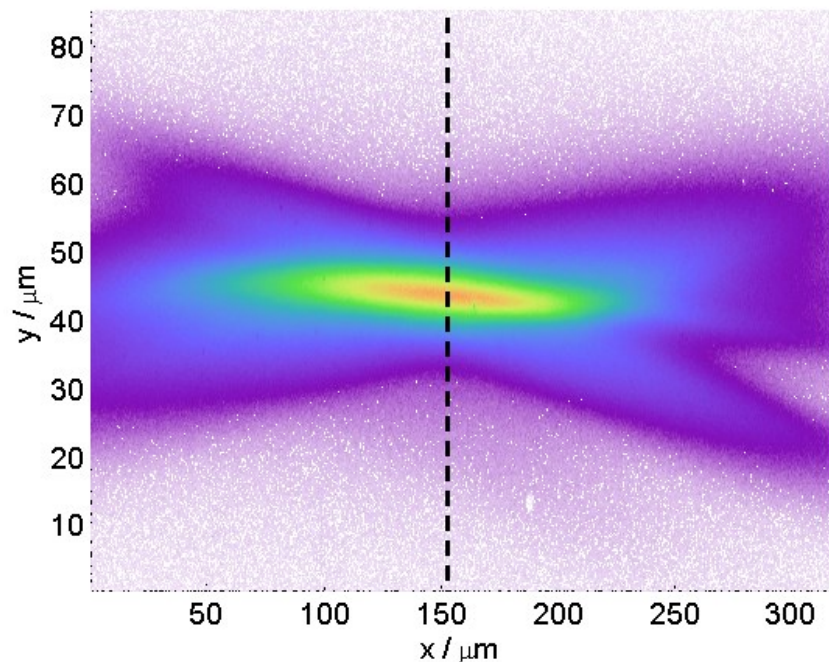
$f = 26.90 \text{ mm}$

NA = 0.19 (nominal)



Micrometer Beam Size Measurement

measured beam image



horizontal beam profile

→ affected by OTR-like 90° observation geometry

vertical beam profile

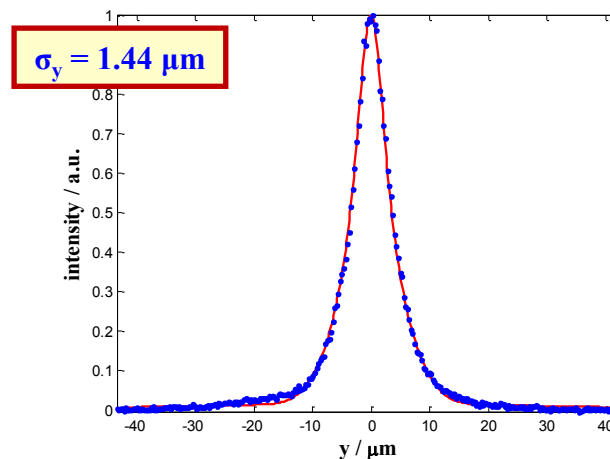
→ affected by depth-of-focus



restriction: analysis only along vertical cut

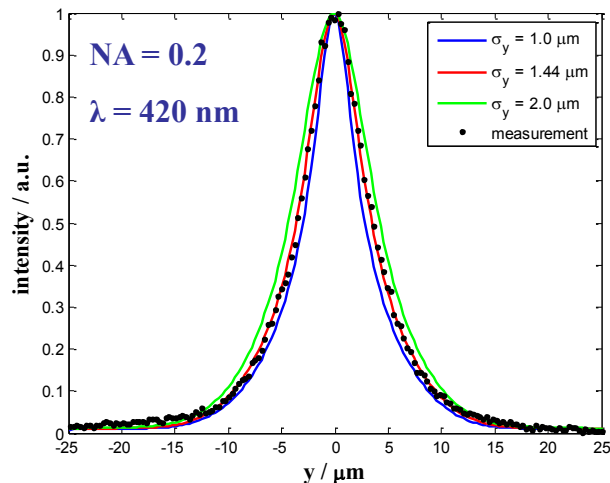
analysis: scintillator model in Zemax[©]

- light emission from single electron represented by line source in LYSO crystal with isotropic light emission
- scintillator properties described by $n(\lambda)$
- Schwarzschild objective replaced by paraxial lens with same f and appropriate NA
- non-sequential ray tracing for 10^8 rays at LYSO peak emission wavelength $\lambda = 420 \text{ nm}$
 - single particle resolution function (SPF)
- SPF convolution with 2D-Gaussian (beam profile)
- vertical cut and comparison



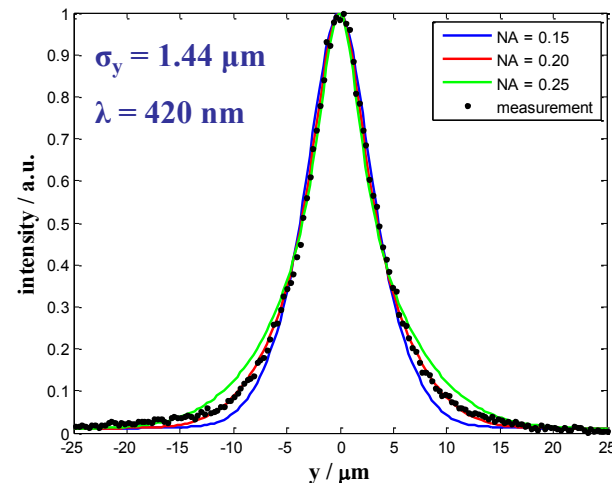
Sensitivity - Parameter Influence

beam size



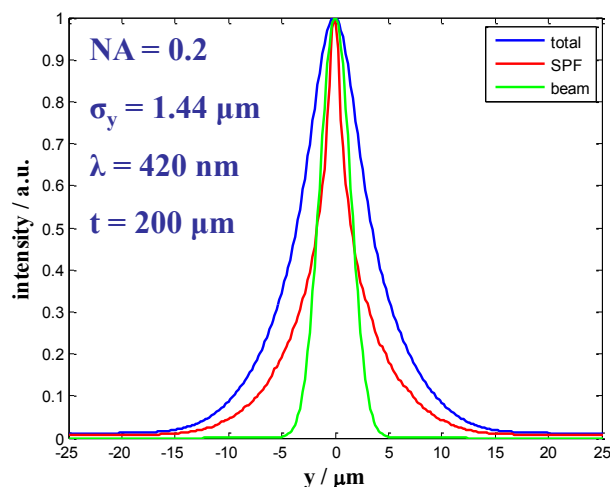
► affects central part of distribution

numerical aperture

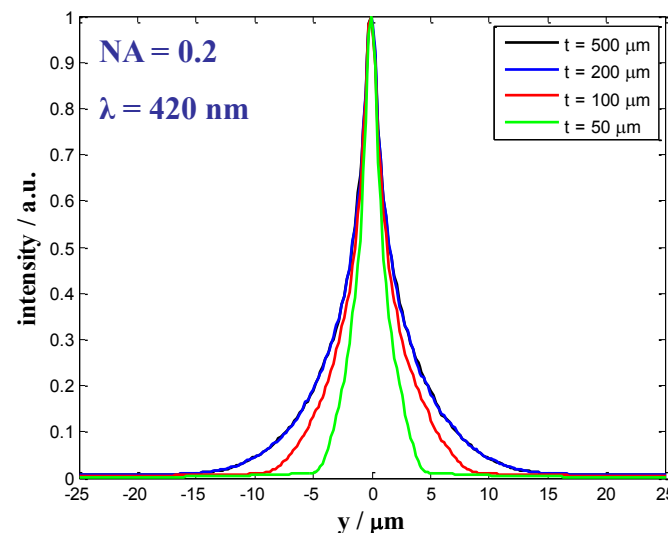
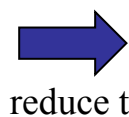


► affects tails of distribution

resolution improvement



► individual contributions



Conclusion and Outlook

- search for high resolution scintillator materials
 - suitable candidate: LYSO:Ce
- influence on observation geometry
 - considerable influence on spatial resolution
 - basic understanding in frame of geometrical light propagation
- micrometer beam size measurements
 - micrometer beam size measured with 200 μm thick LYSO:Ce scintillator
 - analysis requires knowledge of Single Particle Function (SPF)
 - better sensitivity for thinner crystals
- XFEL screen monitors: perturbed beam profiles
 - measured emittance values larger than expected
 - assumption: scintillator effect
 - caused by high *ionization track density* due to *primary beam density*
 - quenching of excitation centers
 - search for better scintillator materials
 - next weekend : beam test at XFEL

e/ γ -Response of Scintillators

- scintillators used for γ -ray beam profile measurements

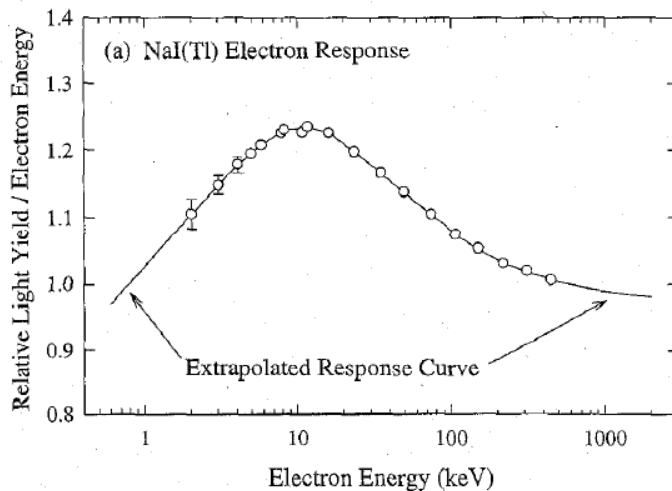
- X-ray converter for CCDs → e.g. for pinhole camera



difference in scintillator response between *electrons* and *photons* ?

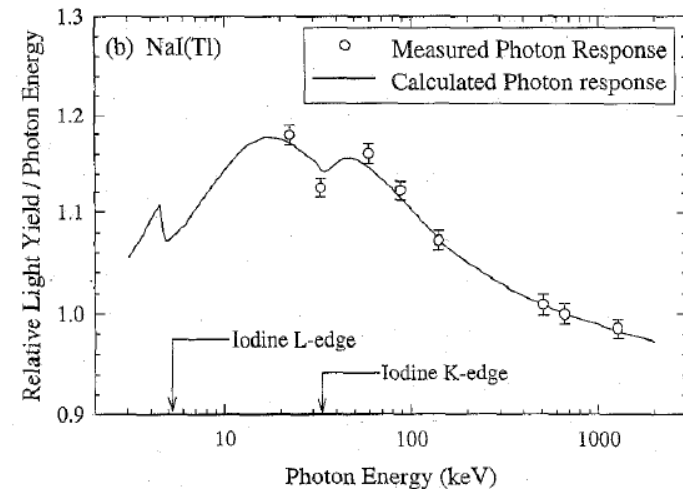
- electron response

- collisional stopping power
 - several small interactions
 - mainly with outer shell electrons



- photon response

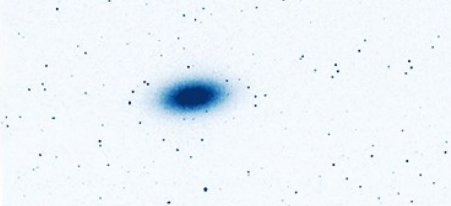
- photo effect
 - single interaction, predominantly with inner shells
 - complex cascade structure



B.D. Rooney and J.D. Valentine, IEEE Trans. Nucl. Sci. **44** (1997) 509

- smooth electron response

- photon response with substructure



Comments on Digital Camera Systems for Beam Diagnostics Applications

Gero Kube
DESY (Hamburg)

- Charge-Coupled Devices (CCD)
- CMOS Imaging Sensor (CIS)
- Sensor Performance Study



only Cameras for
Machine Vision

CCD Working Principle

● image generation with CCD: 4 stage process

- charge generation
- charge collection
- charge transfer
- charge measurement

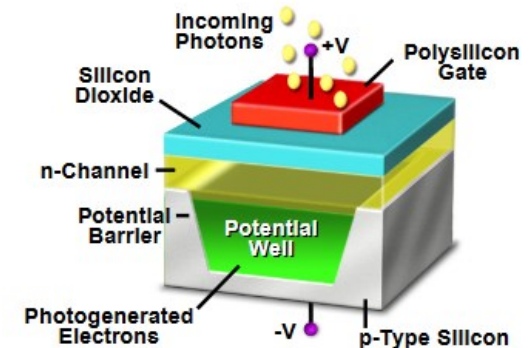
● charge generation & collection: fundamental light-sensing unit

- metal oxide semiconductor (MOS) capacitor
- operated as a photodiode and storage device
- photo effect: conversion of incoming photons into charge
- reverse bias operation

→ electrons migrate to area underneath positively

charged gate electrode

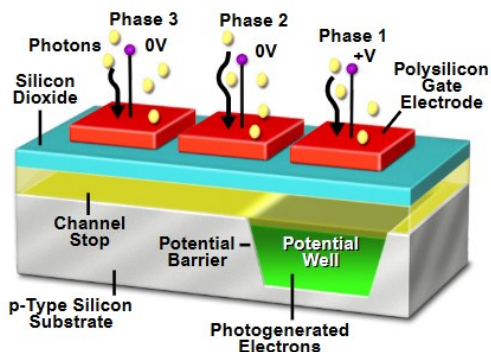
(well capacity: $1000-2000 \text{ e}^-/\mu\text{m}^2$)



<https://www.microscopyu.com>

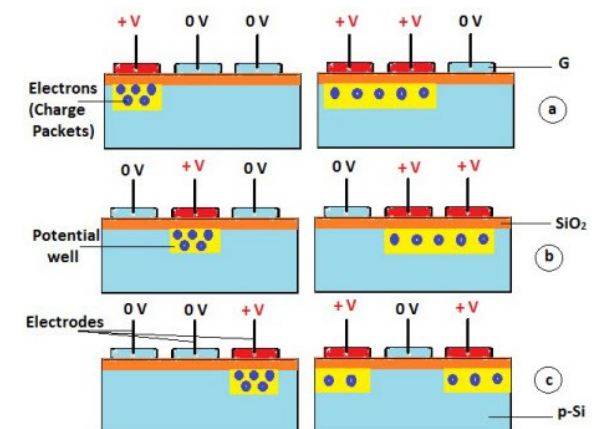
● charge transfer

- CCD sense element (pixel) structure



<https://www.microscopyu.com>

- line array of pixels forms transfer register
- **transfer** of charge packets **according to voltage** applied to the gate terminals
- requires overlap of depletion region in transfer direction



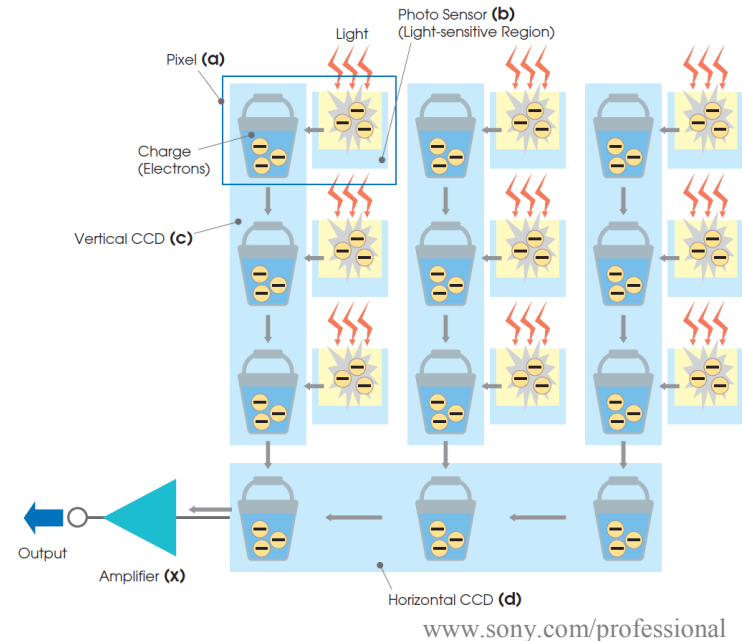
<https://www.elprocus.com/know-about-the-working-principle-of-charge-coupled-device/>

CCD Working Principle (2)

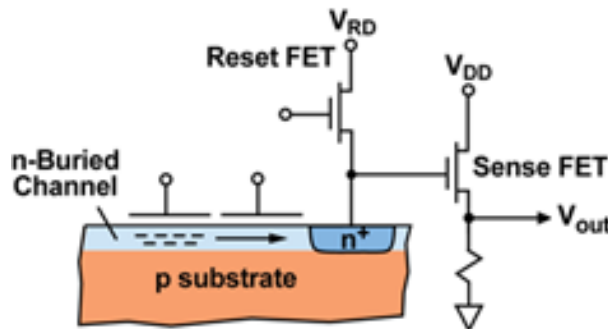
● charge transfer (cntd.)

- ▶ CCD array is series of column registers
 - charge kept within rows by channel stops
- ▶ end of each column: horizontal shift register
 - collects a line at a time
 - transports charge packets in serial fashion to output amplifier
 - entire horizontal register has to be clocked out before next line enters
 - requires separate horizontal (fast) / vertical (slow) clocks
- ▶ gate voltages $\sim 8 \dots 15$ V required for creation of depletion wells
 - rapidly turn on/off for charge transport → high power consumption

water bucket analogy:



● charge measurement



- ▶ n^+ : *floating diffusion* or *sense node*
 - region in active silicon (diffusion) region, electrically isolated
 - potential determined by the amount of stored charge and capacitance
- ▶ Sense FET: *source follower* configuration (impedance transformation)
 - buffers poor voltage source (high R_i) into nearly ideal one (low R_i), $A \sim 1$
- ▶ Correlated Double Sampling (CDS): measure after reset & charge dump + subtract
 - reduce signal fluctuations

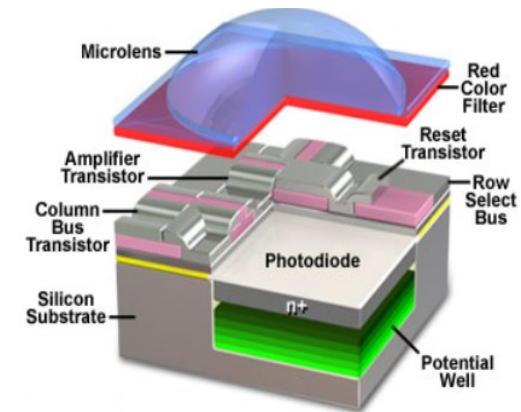
CMOS Working Principle

● CMOS : Complementary Metal-Oxide-Semiconductor

- well established technology for constructing integrated circuits
 - evolved to smaller circuit sizes → lower power consumption

● CMOS Imaging Sensor (CIS): active pixel sensor most popular design

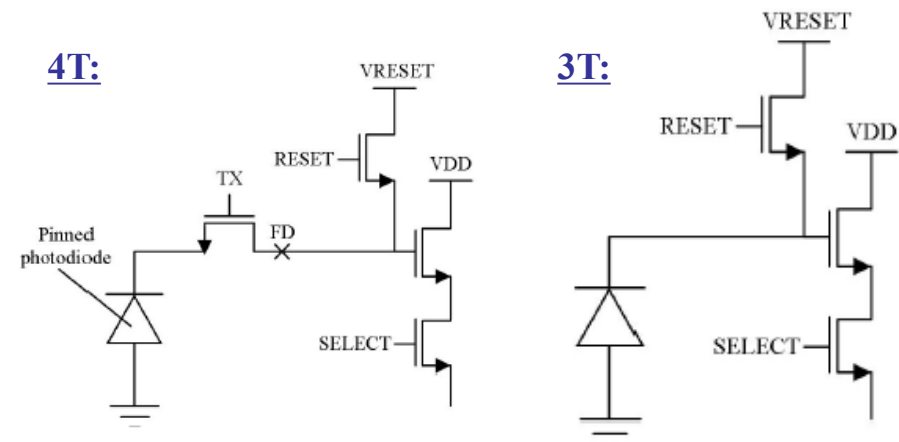
- photodiode and readout amplifier incorporated into each pixel
 - CIS contains analogue and digital components
- accumulated **charge** converted into **voltage** inside pixel
- voltage conversion similar to CCD
 - source follower & voltage signal amplification (otherwise too small to be transferred)
- if pixel selected
 - pixel readout via external readout circuitry



<https://www.olympus-lifescience.com/en/microscope-resource/primer/>

● pixel architecture

- **3T**(ransistors): Reset, Source Follower, Select
 - small pixels, for consumer market (cell phone,...)
 - **rolling shutter** (problems with moving object)
- **4T**: ...+ Transfer Gate TX (and Floating Diffusion)
 - higher sensitivity (smaller C) & lower noise (CDS)
 - **global shutter** (allows snapshots)

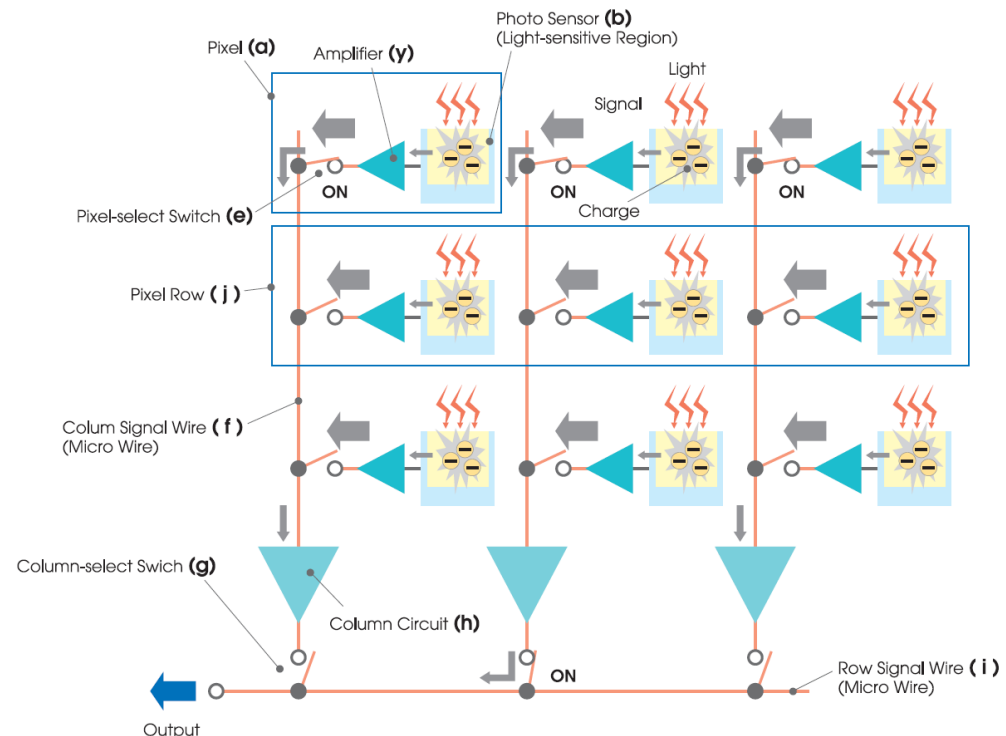


R. Coath et al., Advanced Pixel Architectures for Scientific Image Sensors, 2009

CMOS Working Principle (2)

● CIS structure and readout

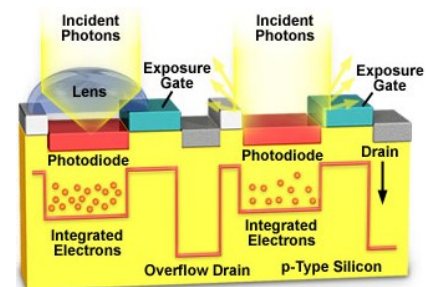
- each pixel (a)
 - amplified voltage signal
- pixel-select switch (e, Select Transistor) turned on
 - outputs amplified voltages of all pixels in selected row (j) to their respective column circuit (h, sample & hold)
 - slow speed parallel readout
- column-select switch (g) turned on from left to right
 - signal voltages of each pixel in row are read out
 - high speed serial readout
- repeat operation for all rows from top to bottom



www.sony.com/professional

● consequences

- voltage transfer
 - faster than charge transfer in CCDs (~ 100 fps vs. 20 fps)
- windowing
 - readout of sub-structures → even faster readout
- reduced fill factor (amplifier on CIS)
 - micro-lenses



<http://micro.magnet.fsu.edu/primer/>

Comparison CCD versus CMOS

mechanisms of CCD and CMOS image sensors

www.sony.com/professional

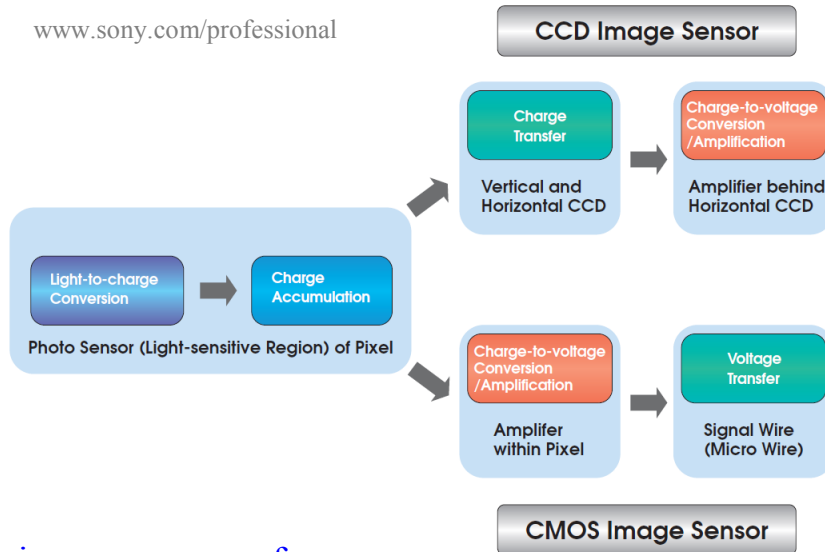


image sensor performance

Photonics Spectra, Issue January 2001

- responsivity
- dynamic range
- uniformity
- shuttering
- speed
- windowing
- antiblooming
- biasing & clocking

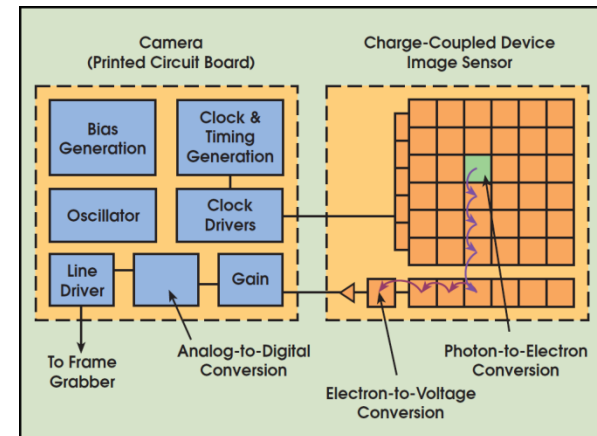


better image sensor type ???

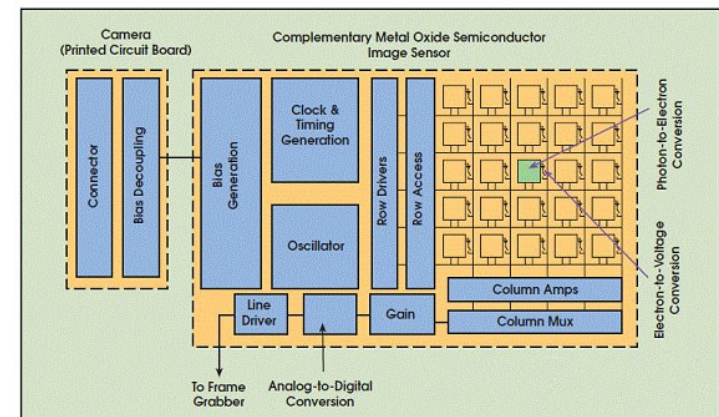
Sony announced in March 2015 that it was discontinuing its entire line of CCD sensors...

camera architecture

CCD



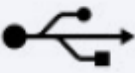
























CMOS



Photonics Spectra, Issue January 2001

Digital Camera Interfaces

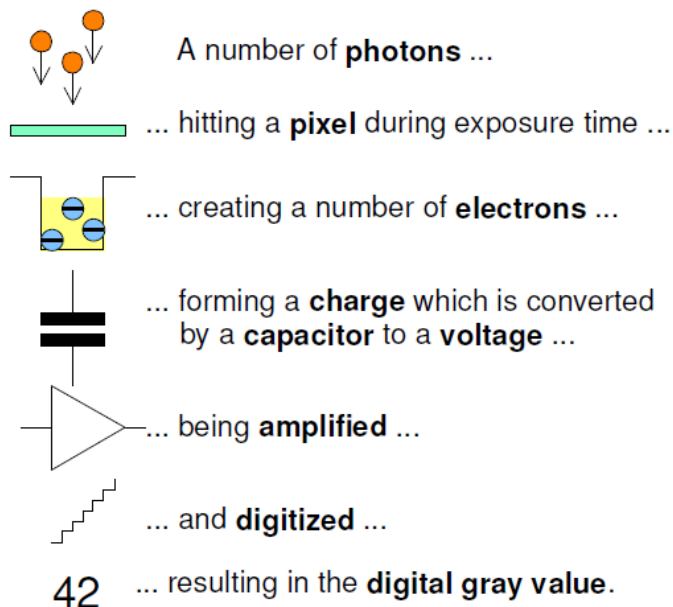
- various interfaces in overview

| Interface | Cable length | Band width maximum in MB/s. | Multi-camera | Cable costs | „Real-time“ | „Plug & Play“ |
|---|--------------|-----------------------------|---|--|---|---|
|  USB 2.0 | 5m | 40 |  |  |  |  |
|  FireWire | 4.5m | 64 |  |  |  |  |
|  GiGE VISION | 100 m | 100 |  |  |  |  |
|  USB ³ VISION | 8 m | 350 |  |  |  |  |
|  CAMERA Link | 10 m | 850 |  |  |  |  |

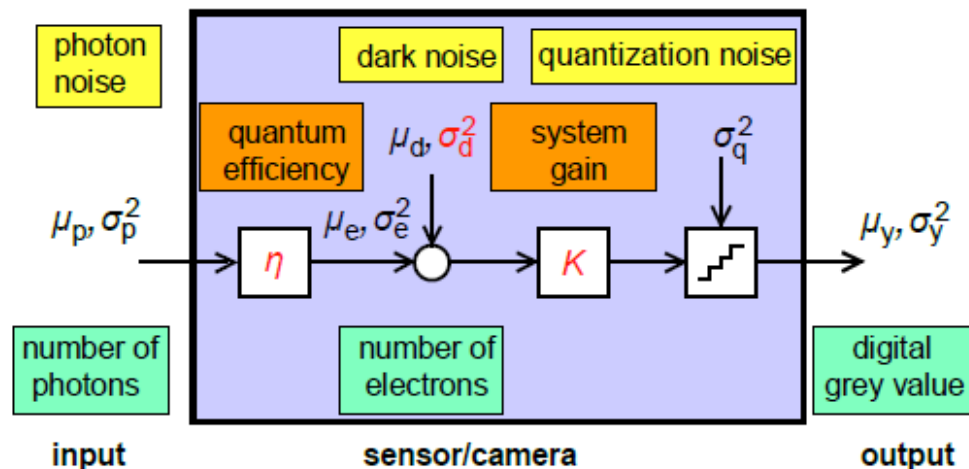
Basler White Paper1505, www.baslerweb.com

Testing Camera Performance

physical camera model



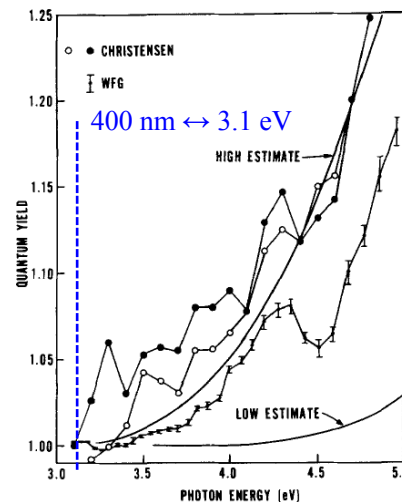
mathematical model of single pixel



EMVA Standard 1288, Release 3.1, Release Candidate (2012), www.emva.org

mathematical model: validity

- amount of photons depend on radiative energy density
- sensor linearity (valid for $\lambda > 400$ nm)
- noise sources are stationary and white
- only total quantum efficiency depends on λ
- only dark current depends on temperature



F.J. Wilkinson et al.,
 J. Appl. Phys. 54 (1983)
 1172

Photon Transfer Method

basic assumptions

- number of photons/electrons: stochastic values
 - characterization by mean/variance

mean number of photons:

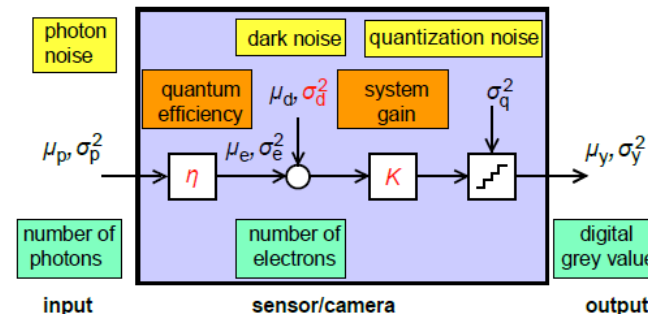
$$\mu_p = \sigma_p^2$$

mean number of electrons:

$$\mu_e = \eta \mu_p$$

CCD output

- grey value y
 - unit DN (digital number)
- simplification
 - neglect quantization noise σ_q



$$\sigma_e^2 = \mu_e = \eta \mu_p$$

(Poisson distributed)



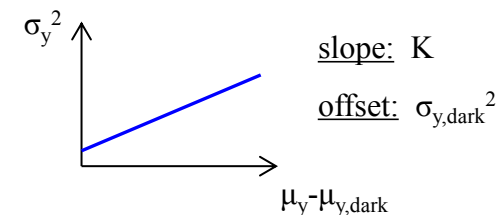
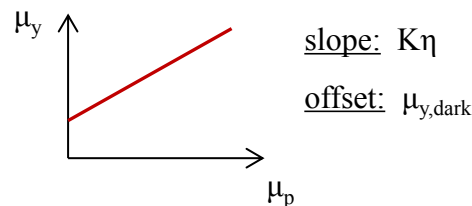
$$\mu_y = K(\mu_e + \mu_d) = K \eta \mu_p + \mu_{y,dark}$$

$$\sigma_y^2 = K^2(\sigma_e^2 + \sigma_d^2) = K(\mu_y - \mu_{y,dark}) + \sigma_{y,dark}^2$$

Photon Transfer Method

measurement

- μ_y, σ_y^2 as function of μ_p



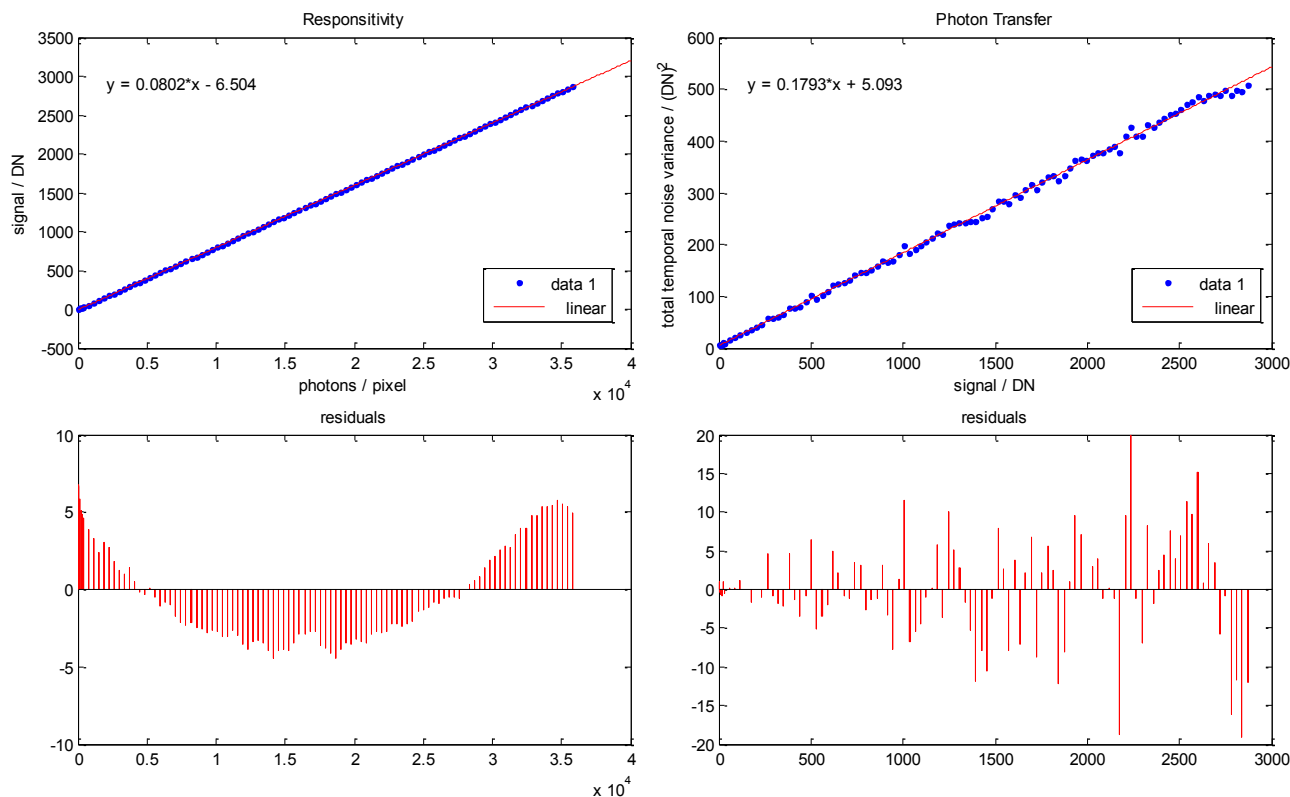
PT Measurements

● **CCD under test** → Basler Aviator avA1600-gm

- for each exposure time (μ_p): take 10 images
- select ROI: 50 x 50 pixels

→ determine mean gray value and noise variance: μ_y, σ_y^2

● **analysis**



● **results**

➤ overall system gain

$$K = 0.1793 \text{ DN/e}^-$$

$$\rightarrow K^{-1} = 5.6 \text{ e}^-/\text{DN}$$

➤ QE @ 470nm

$$K \eta = 0.0802$$

$$\rightarrow \eta = 0.447$$

➤ dark noise

$$\sigma_{y,\text{dark}}^2 = (5.093 \text{ DN})^2$$

$$\rightarrow \sigma_d = 12.6 \text{ e}^-$$

➤ EMVA 1288 data sheet

| Item | Symbol | Typ. ¹ | Unit |
|----------------------------------|----------------------|-------------------|--------------------|
| Temporal Noise Parameters | | | |
| Total Quantum Efficiency (QE) | η | 40 | % |
| Inverse of Overall System Gain | $\frac{1}{K}$ | 4.8 | e ⁻ /DN |
| Temporal Dark Noise | σ_{d0} | 11 | e ⁻ |
| Saturation Capacity | $\mu_{e,\text{sat}}$ | 18500 | e ⁻ |

www.baslerweb.com

(QE @ 545 nm)

Signal-to-Noise Ratio

• measure for signal quality

- › usually in logarithmic representation

$$SNR_y(\mu_p) = \frac{\mu_y - \mu_{y,dark}}{\sigma_y} = \frac{\eta\mu_p}{\sqrt{\eta\mu_p + \sigma_d^2}}$$



$$ld(SNR_y) = ld(\eta) + ld(\mu_p) - \frac{1}{2} ld(\eta\mu_p + \sigma_d^2)$$

- › ideal sensor: $\eta = 1, \sigma_d = 0$

$$ld(SNR_y) = \frac{1}{2} ld(\mu_p)$$

→ pure shot noise from photons, i.e. $SNR_y = \sqrt{\mu_p}$

• limiting cases

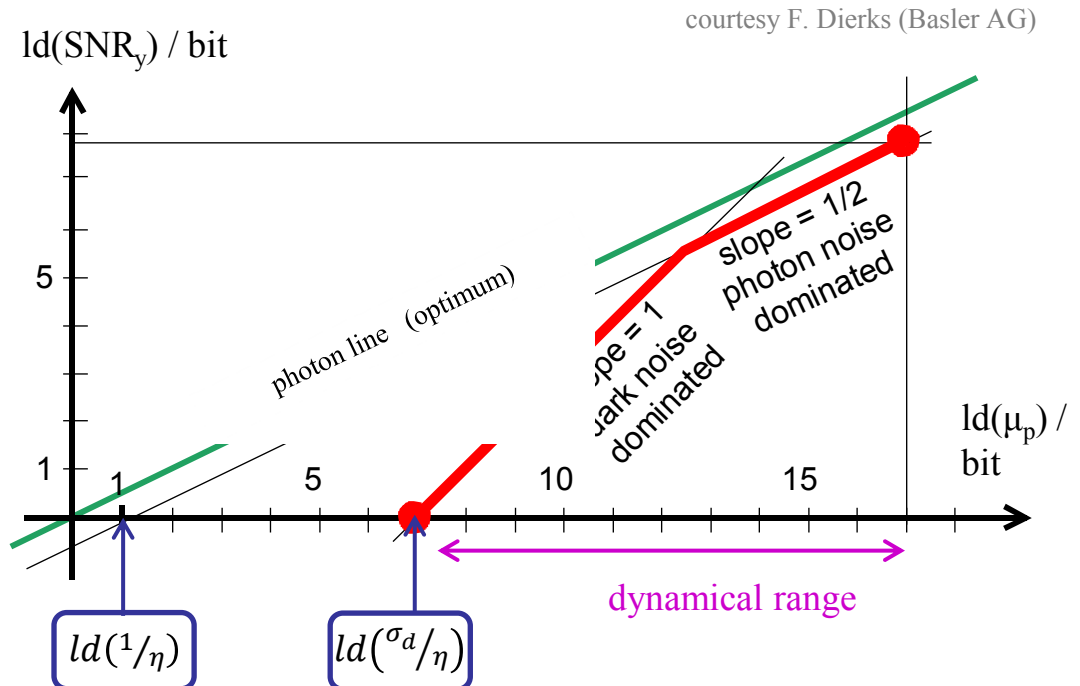
- › shot noise dominated: $\eta\mu_p \gg \sigma_d^2$

$$ld(SNR_y) = \frac{1}{2} ld(\mu_p) + \frac{1}{2} ld(\eta)$$

- › dark noise dominated: $\eta\mu_p \ll \sigma_d^2$

$$ld(SNR_y) = ld(\mu_p) + ld(\eta/\sigma_d^2)$$

- › intersection with $SNR_y = 1$:



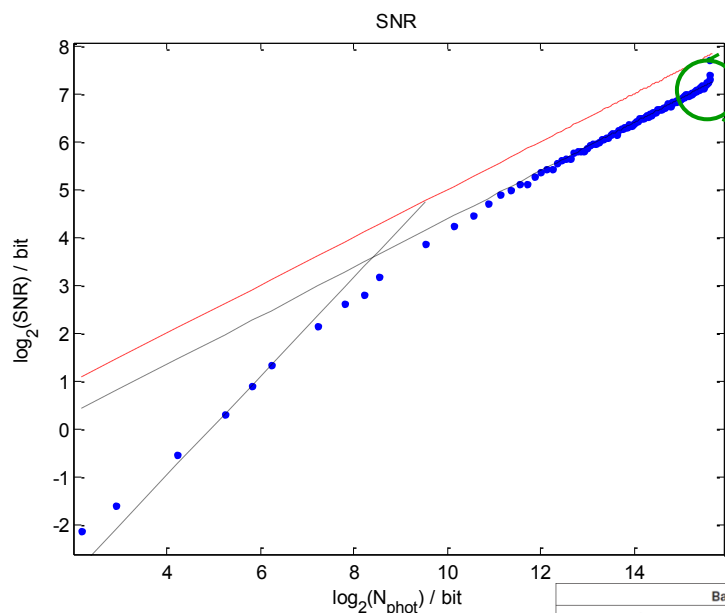
Signal-to-Noise Analysis

● CCD under test → Basler Aviator avA1600-gm

➤ same data set as before

● QE (η) and dark noise (σ_d)

➤ from intersection with $\text{Id}(\text{SNR})$ axis → $\text{SNR} = 1$



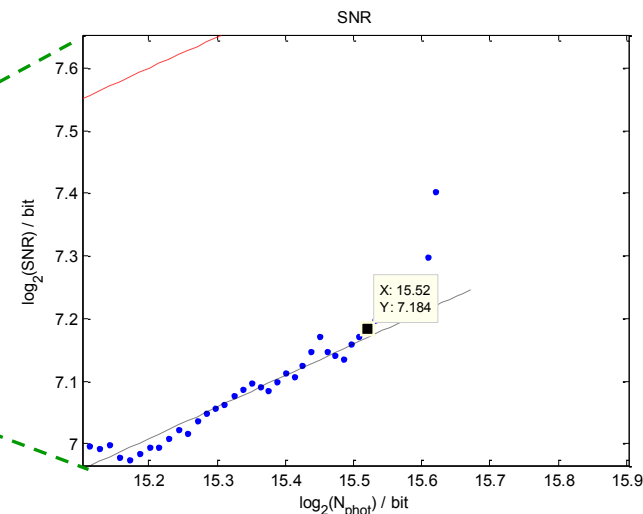
www.baslerweb.com

| Basler avA1600-50gm | | | | |
|----------------------------------|---------------------------------|-------------------|--------------------------------|----------------------------|
| Item | Symbol | Typ. ¹ | Unit | Remarks |
| Temporal Noise Parameters | | | | |
| Total Quantum Efficiency (QE) | η | 40 | % | $\lambda = 545 \text{ nm}$ |
| Inverse of Overall System Gain | $\frac{1}{K}$ | 4.8 | $\frac{\text{e}^-}{\text{DN}}$ | |
| Temporal Dark Noise | σ_{d0} | 11 | e^- | |
| Saturation Capacity | μ_{sat} | 18500 | e^- | |
| Derived Parameters | | | | |
| Absolute Sensitivity Threshold | $\mu_{\text{p,min}}$ | 28 | p^- | $\lambda = 545 \text{ nm}$ |
| Dynamic Range | $\text{DYN}_{\text{out,bit}}$ | 10.7 | bit | |
| Maximum SNR | $\text{SNR}_{\text{q,max,bit}}$ | 7.1 | bit | |
| | $\text{SNR}_{\text{q,max,dB}}$ | 42.7 | dB | |

$$\eta = 0.40$$

$$\sigma_d = 12.2 \text{ e}^-$$

● dynamical range (DR) and saturation (ST)



➤ minimum number of photons

$$\mu_{\text{p,min}} = \sigma_d / \eta = 30.6$$

➤ maximum number of photons

$$\mu_{\text{p,sat}} = 2^{15.52} = 46988$$

$$\text{DR} = 1535 = 63.7 \text{ dB} = 10.6 \text{ bit}$$

$$\text{ST} = \mu_{\text{p,sat}} \eta = 18800 \text{ e}^-$$